# ECE 205 "Electrical and Electronics Circuits" 

## Spring 2024 - LECTURE 21 <br> MWF - 12:00pm

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## Lectures 21 - Summary

## Learning Objectives

1. Solution of circuit problems with phasors

## Quiz 2 - Grade Distribution



## Quiz 2 - Statistics

Number of students ..... 293
Mean score ..... 81\%
Standard deviation ..... 24\%
Median score ..... 91\%
Minimum score ..... 2\%
Maximum score ..... 100\%
Number of 0\%0 (0\% of class)Number of 100\%30 (10\% of class)

## EXAMPLES

# Resonance in RLC circuits 

Let's take this opportunity also to retrace the steps leading to phasors, for review.

Time-differential equations for time harmonic signals can be transformed into algebraic equations for phasors.


In the previous lecture we found that this circuit is described by a second order differential equation

$$
\frac{d v(t)}{d t}=L \frac{d^{2} i(t)}{d t^{2}}+R \frac{d i}{d t}+\frac{1}{C} i(t)
$$

Time-differential equations for time harmonic signals can be transformed into algebraic equations for phasors.

Time
domain

$$
\frac{d v(t)}{d t}=L \frac{d^{2} i(t)}{d t^{2}}+R \frac{d i}{d t}+\frac{1}{C} i(t)
$$

Phasor


$$
\begin{aligned}
& \widetilde{V}=\mathrm{j} \omega L \widetilde{I}+R \tilde{I}+\frac{1}{\mathrm{j} \omega C} \widetilde{I} \\
& \widetilde{V}=\underbrace{\left(R+\mathrm{j} \omega L-\mathrm{j} \frac{1}{\omega C}\right)}_{\text {Impedance } Z} \widetilde{I}
\end{aligned}
$$

$$
\widetilde{V}=\left(R+\mathrm{j} \omega L-\mathrm{j} \frac{1}{\omega C}\right) \widetilde{I}=Z \widetilde{I}
$$

is a new form of Ohm's law!


The equation is easily solved

$$
\begin{gathered}
\widetilde{V}=Z \widetilde{I} \quad \rightarrow \quad \widetilde{I}=\frac{\widetilde{V}}{Z} \\
\widetilde{I}=\frac{\widetilde{V}}{\left(R+\mathrm{j} \omega L-\mathrm{j} \frac{1}{\omega C}\right)}=I_{0} \exp \left(\mathrm{j} \theta_{I}\right)
\end{gathered}
$$

to obtain the unknowns $I_{0}$ and $\theta_{I}$
The time-dependent solution is obtained from a backward phasor transformation (anti-transform)

$$
\begin{aligned}
\boldsymbol{i}(t)= & \mathfrak{R e}\left\{\boldsymbol{I}_{\mathbf{0}} \exp \left(\mathrm{j} \theta_{I}\right) \exp (\mathrm{j} \omega \mathrm{t})\right\} \\
& =\boldsymbol{I}_{\mathbf{0}} \cos \left(\omega \boldsymbol{\omega}+\theta_{I}\right)
\end{aligned}
$$

The phasor formalism has provided a convenient way to solve time-harmonic problems in steady state, without differential equations (which are only needed for transients).

The exponential representation of phasors allows immediate separation of frequency and phase information.


The simple RLC circuit example with elements in series illustrates clearly the main properties of an impedance

- The resistance is not function of $\omega$
- The inductive component is proportional to $\omega$
- The capacitive component is inversely proportional to $\boldsymbol{\omega}$


## Inductive components are positive Capacitive components are negative

In series connection, inductive and capacitive components simply add up.

## Resonance

At a certain frequency $\omega_{r}$ the magnitudes of the two reactive terms are equal, so they cancel out (together, they behave like a short circuit)

$$
Z=R+\mathrm{j} \omega_{r} L-\mathrm{j} \frac{1}{\omega_{r} C}=R
$$

$\rightarrow$ The impedance becomes purely resistive.

$$
\omega_{r} L=\frac{1}{\omega_{r} C}
$$

$$
\omega_{r}=\frac{1}{\sqrt{L C}}
$$

## The peak value of the current is maximum at resonance

Example:

$$
\begin{aligned}
V_{0} & =10 \mathrm{~V} & & R=1 \Omega \\
L & =1 \mathrm{H} & & C=1 \mathrm{~F}
\end{aligned}
$$

Consider now a circuit with $L$ and $C$ in parallel


$$
Z_{i n}=R+\left(\frac{1}{\mathrm{j} \omega L}+\mathrm{j} \omega C\right)^{-1}=R+\frac{\mathrm{j} \omega L}{1-\omega^{2} L C}
$$

$$
Z_{i n}=R+\left(\frac{1}{\mathrm{j} \omega L}+\mathrm{j} \omega C\right)^{-1}=R+\frac{\mathrm{j} \omega L}{1-\omega^{2} L C}
$$

When:

$$
\begin{array}{cc}
\omega=\mathbf{0} & \boldsymbol{Z}_{\text {in }}=\boldsymbol{R} \\
& \boldsymbol{Z}_{\text {in }} \rightarrow \infty \\
\omega=\frac{1}{\sqrt{L \boldsymbol{C}}} & \begin{array}{l}
\text { resonance } \\
\text { condition }
\end{array} \\
\hdashline \boldsymbol{\omega} \rightarrow \infty & \boldsymbol{Z}_{\text {in }}=\boldsymbol{R}
\end{array}
$$

At the resonance condition, the reactance (parallel of $L$ and $C$ ) behaves like an open circuit and no current can flow.

The peak value of the current is zero at resonance

$$
\begin{array}{cc}
V_{0}=10 \mathrm{~V} & R=1 \Omega \\
L=1 \mathrm{H} & C=1 \mathrm{~F}
\end{array}
$$

$$
|\widetilde{I}|=\frac{|\widetilde{V}|}{\sqrt{R^{2}+\left(\frac{\omega L}{1-\omega^{2} L C}\right)^{2}}}
$$



Find phasors $V_{1}, V_{2}, V_{3}, I_{1}, I_{2}, I_{3}$ (We can drop the wavy hat ${ }^{\sim}$ now)


## $V_{1}=2 V$

By inspection


Node 2 KCL $\quad \frac{V_{2}-V_{1}}{-\mathrm{j} 1}+\frac{V_{2}}{1}+1 \angle 90^{\circ}=\mathbf{0}$

## $V_{1}=2 V$



Node 2 KCL $\quad \frac{V_{2}-V_{1}}{-\mathrm{j} 1}+\frac{V_{2}}{1}+1 \angle 90^{\circ}=0$
$\mathrm{j} V_{2}-2 \mathrm{j}+V_{2}+\mathrm{j} 1=0 \quad \Rightarrow \quad V_{2}(1+\mathrm{j})=\mathrm{j} 1$

$$
V_{2}=\frac{\mathbf{j} 1}{(1+\mathbf{j})}=\frac{\mathbf{j} 1(1-\mathbf{j})}{(1+\mathbf{j})(1-\mathbf{j})}=\frac{1+\mathbf{j}}{2}=0.5+\mathbf{j} 0.5
$$

## $V_{1}=2 V$

## $V_{2}=0.5+j 0.5 \mathrm{~V}$



Node 3 KCL

$$
\frac{V_{3}}{\mathrm{j} 2}+\frac{V_{3}-2}{2} \underbrace{-1 \angle 90^{\circ}=0}
$$

## $V_{1}=2 V$

## $V_{2}=0.5+\mathbf{j} 0.5 \mathrm{~V}$



Node 3 KCL
$\frac{V_{3}}{\mathrm{j} 2}+\frac{V_{3}-2}{2} \underbrace{-1 \angle 90^{\circ}}=0$

$$
-\mathrm{j} \frac{1}{2} V_{3}+\frac{1}{2} V_{3}-1-\mathrm{j} 1=0 \Rightarrow V_{3}=\frac{1+\mathrm{j} 1}{(1-\mathrm{j} 1) / 2}
$$

$$
V_{3}=\frac{2(1+\mathrm{j} 1)(1+\mathrm{j} 1)}{2}=\mathrm{j} 2 \mathrm{~V}
$$

## $V_{1}=2 V$

## $V_{2}=0.5+\mathrm{j} 0.5 \mathrm{~V}$

$$
V_{3}=\mathrm{j} 2 \mathrm{~V}
$$

Currents

$\overbrace{I_{4}=I_{1}-I_{2}}^{\text {KCL node } 1}=\frac{V_{1}-V_{2}}{-j 1}=\frac{2-(0.5+j 0.5)}{-j 1}$
$=0.5+j 1.5 \mathrm{~A}$

$$
\begin{aligned}
& V_{1}=2 \mathrm{~V} \\
& V_{2}=0.5+\mathrm{j} 0.5 \mathrm{~V} \\
& V_{3}=\mathrm{j} 2 \mathrm{~V}
\end{aligned}
$$

Currents


$$
I_{4}=I_{1}-I_{2}=0.5+\mathrm{j} 1.5 \mathrm{~A}
$$

$$
I_{2}=\frac{V_{1}-V_{3}}{2}=\frac{2-\mathrm{j} 2}{2}=1-\mathrm{jA}
$$

$$
\begin{aligned}
I_{1}=I_{4}+I_{2} & =(0.5+\mathrm{j} 1.5)+(1-\mathrm{j}) \\
& =1.5+\mathrm{j} 0.5 \mathrm{~A}
\end{aligned}
$$

## $V_{1}=2 V$

## $V_{2}=0.5+j 0.5 \mathrm{~V}$

$$
V_{3}=\mathrm{j} 2 \mathrm{~V}
$$

## Currents

$$
\begin{aligned}
& I_{1}=1.5+\mathrm{j} 0.5 \mathrm{~A} \\
& \hline I_{2}=1-\mathrm{j} \mathrm{~A} \\
& \hline
\end{aligned}
$$


${ }^{K C L}$ at Node $3 \quad I_{3}-I_{2}-1 \angle 90^{\circ}=0$

$$
I_{3}-(1-\mathrm{j} 1)-\mathrm{j} 1=0
$$

Also: $I_{3}=V_{3} / \mathbf{j} 2=\mathbf{j} 2 / \mathbf{j} 2=1 \longrightarrow I_{3}=1 \mathrm{~A}$

## Source Transformations

The approach we used before works for phasors, too.


$$
I_{S}=\frac{V_{S}}{Z_{S}}
$$

## Source Transformations



## Example

## 1mF


$i_{1}(t)=1 \cos (100 t) A$
$i_{2}(t)=0.5 \cos \left(100 t-90^{\circ}\right) A$
Find $i(t)$

Redraw with Phasors $\quad-\mathbf{j 1 0}$
$\omega=100 \mathrm{rad} / \mathrm{s}$


Source Transformations

## $(4-j 2) \Omega$


$(4-j 2) V$

$1 \angle 0^{\circ} \mathrm{A}$


$$
V_{T}=-\mathrm{j} 0.5(2+\mathrm{j} 4)=(2-\mathrm{j} 1) \mathrm{V}
$$

$(4-\mathrm{j} 2) \Omega \quad-\mathrm{j} 10 \Omega$

KVL


$$
-(4-j 2)-(2-\mathrm{j} 1)+I[(4-\mathrm{j} 2)-\mathrm{j} 10+(2+\mathrm{j} 4)]=0
$$

$$
\Rightarrow \quad(6-j 3)=I(6-j 8)
$$

$$
I=\frac{6-\mathrm{j} 3}{6-\mathrm{j} 8}=\frac{(6-\mathrm{j} 3)(6+\mathrm{j} 8)}{100}=\frac{60+\mathrm{j} 30}{100}=0.6+\mathrm{j} 0.3 \mathrm{~A}
$$

$(4-\mathrm{j} 2) \Omega \quad-\mathrm{j} 10 \Omega$


Find the Thevenin equivalent circuit


## Equivalent impedance



$$
\begin{aligned}
& Z_{e q}=1 \Omega+(2 \Omega+j 2 \Omega) / /(-j 2 \Omega) \\
& Z_{e q}=1+\left[\frac{1}{(2+j 2)}+\frac{1}{(-j 2)}\right]^{-1}=1+\frac{(2+j 2)(-j 2)}{2+j 2-j 2} \\
& Z_{e q}=1+\frac{4-j 4}{2}=3-j 2 \Omega
\end{aligned}
$$

Find open circuit voltage $V_{T H}$


$$
\text { (Supernode) } \begin{array}{|l|l}
\frac{V_{B}-2}{2 \Omega}-\mathrm{j} 1+\frac{V_{B}-V_{A}}{\mathrm{j} 2 \Omega}=0 & \begin{array}{|}
\overline{\overline{2}} \\
V_{C}=V_{B}-2 \mathrm{~V}
\end{array}
\end{array}
$$

$$
\text { (Node A) } \frac{V_{A}-V_{B}}{\mathrm{j} 2 \Omega}+\frac{V_{A}}{-\mathrm{j} 2 \Omega}=0
$$

$$
V_{B}=0
$$

Substituting $V_{B}=\mathbf{0}$ in Supernode KCL:

$$
V_{A}=2-\mathrm{j} 2 \mathrm{~V}
$$

## Thevenin equivalent circuit



