

ECE 205 “Electrical and Electronics Circuits”

Spring 2024 – LECTURE 33

MWF – 12:00pm

Prof. Umberto Ravaioli

2062 ECE Building

Lecture 33 – Summary

Learning Objectives

1. Frequency Response of Circuits
2. Low-Pass Passive Filters

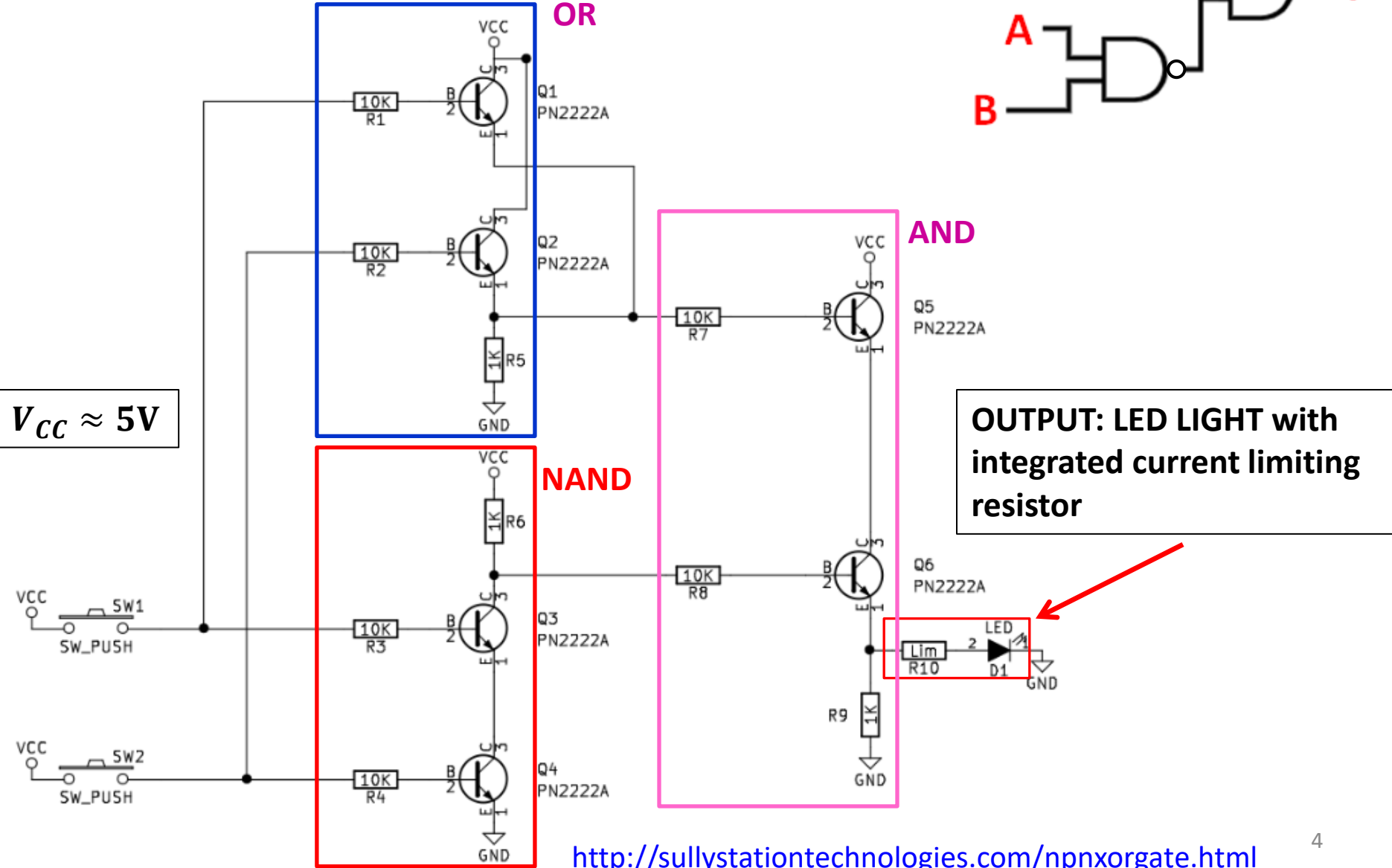
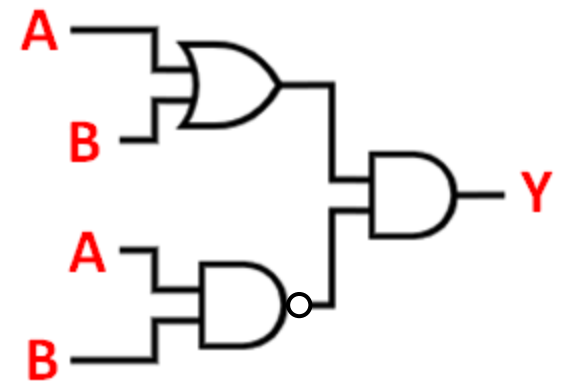
Quiz 4 Reminder

- April 22-24 (next week)
- **5 Questions:**
 - BJT Analysis
 - 2 Questions on $n-p-n$
 - 1 Question on $p-n-p$
 - 1 Question on boolean expression reduction
 - 1 Question on BJT logic circuits
- **Covering from Lectures 24 to Lecture 32**

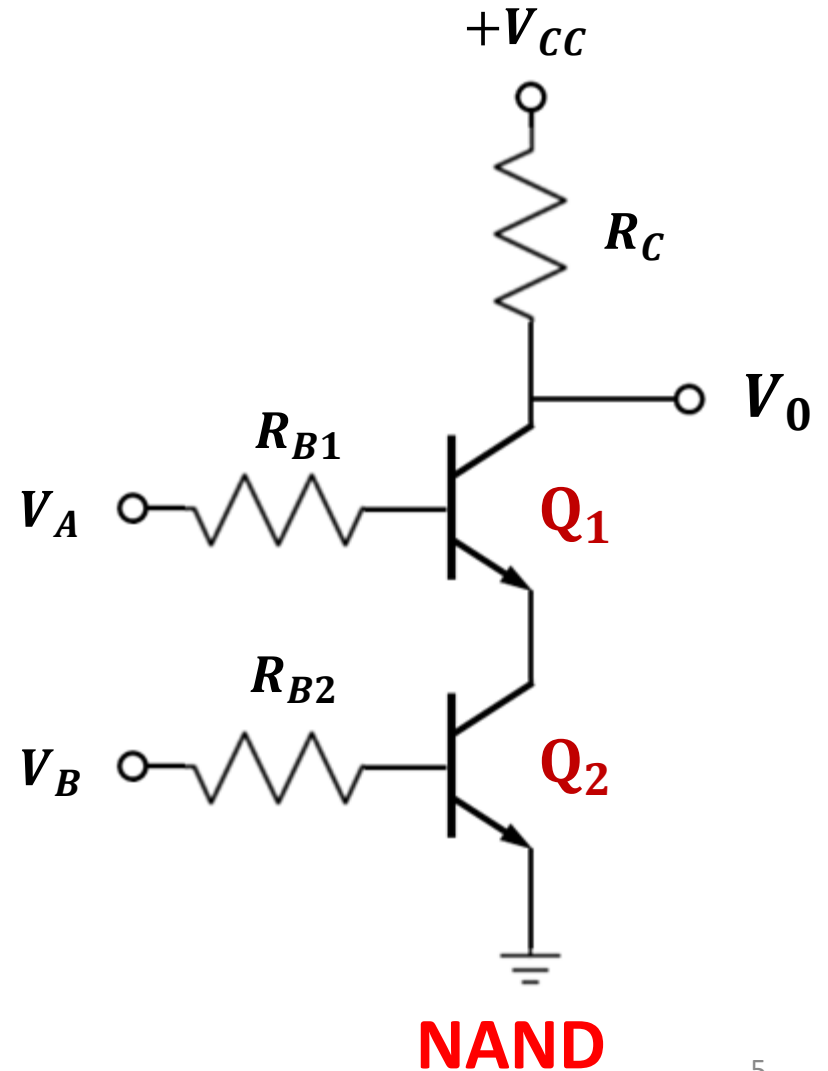
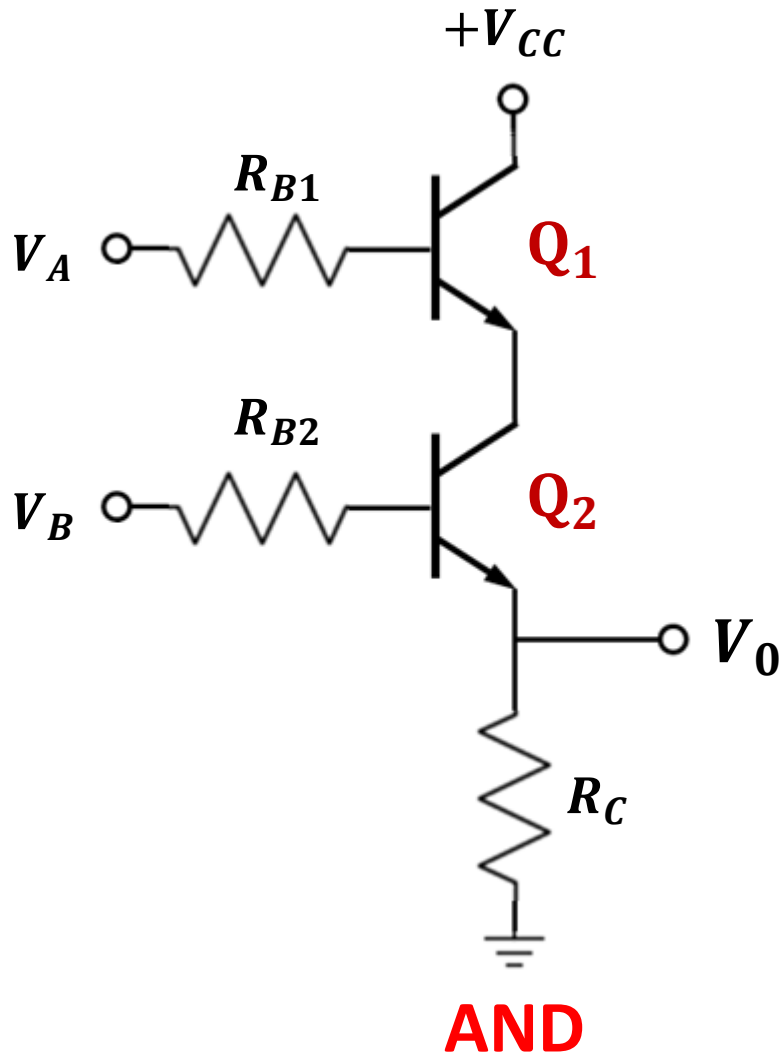
From Lecture 30

$$(A + B) \overline{(AB)}$$

XOR circuit realization with BJT



Minimal implementation

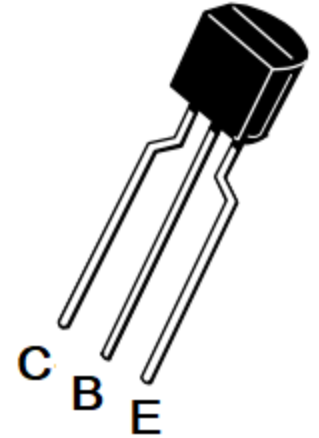


$$V_{BE}(\text{ON}) \approx 0.6 \text{ V}$$

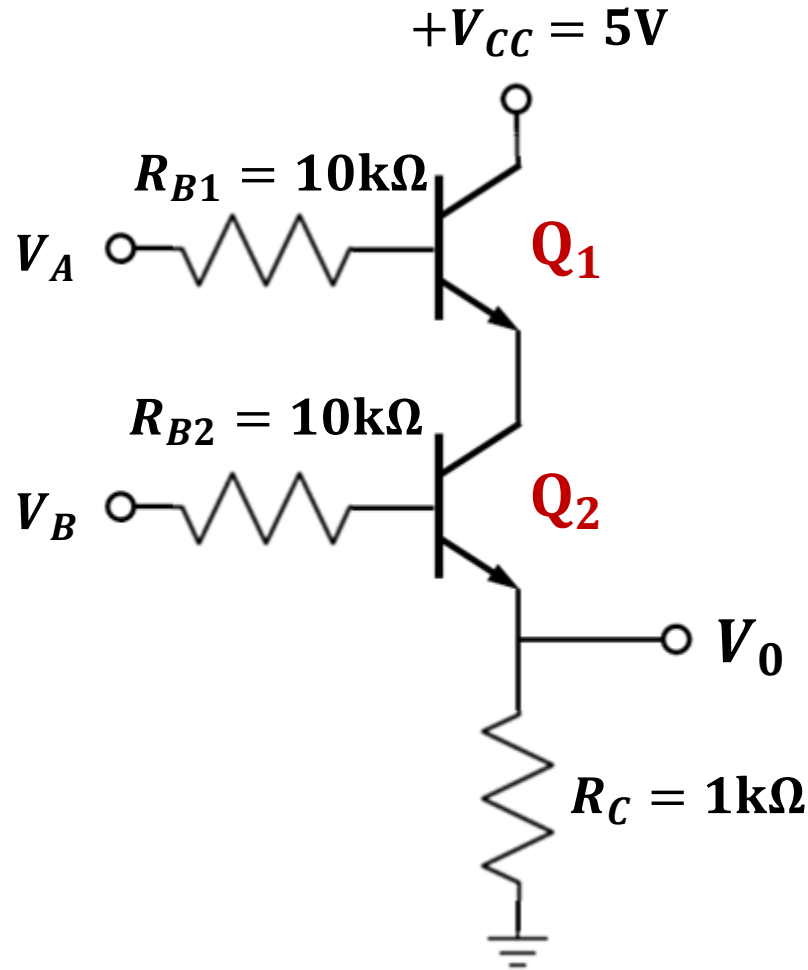
$$V_{CE}(\text{sat}) \approx 0.3 \text{ V}$$

General Purpose PN2222A BJT

$$\beta \approx 100 \text{ to } 300$$



Pick: $\beta = 100$



AND

Two transistors in series

$$V_{BE}(\text{ON}) \approx 0.6 \text{ V}$$

$$V_{CE}(\text{sat}) \approx 0.3 \text{ V}$$

$$\beta = 100$$

$$V_A = V_B = 0 \text{ V}$$

$$V_A = 0 \text{ V}$$

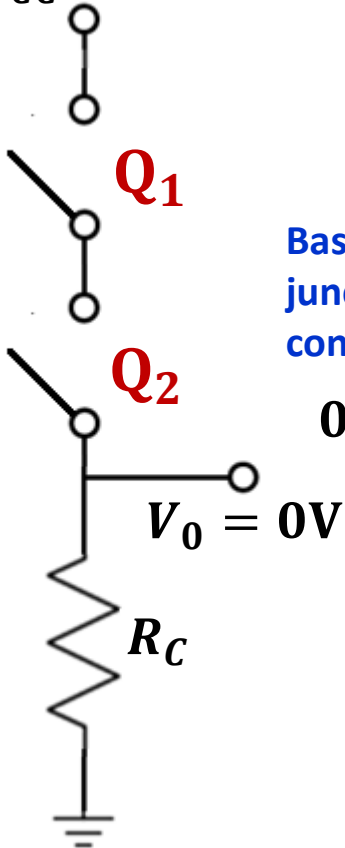
$$V_B = 5 \text{ V}$$

$$V_A = 5 \text{ V}$$

$$V_B = 0 \text{ V}$$

$$V_A = V_B = 5 \text{ V}$$

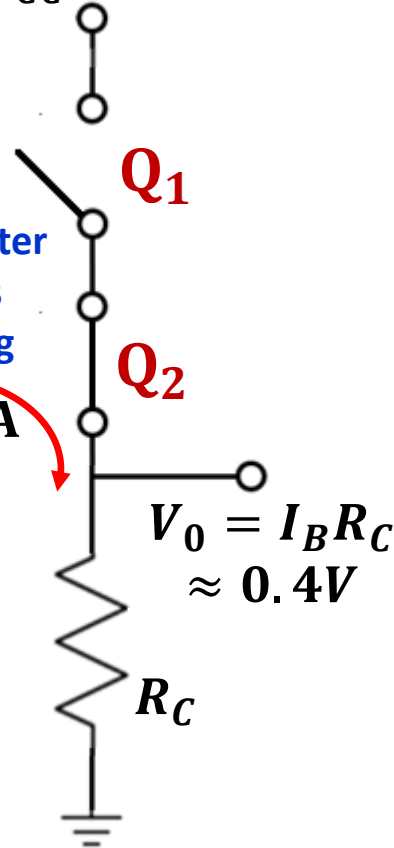
$$+V_{CC} = 5 \text{ V}$$



$$+V_{CC} = 5 \text{ V}$$

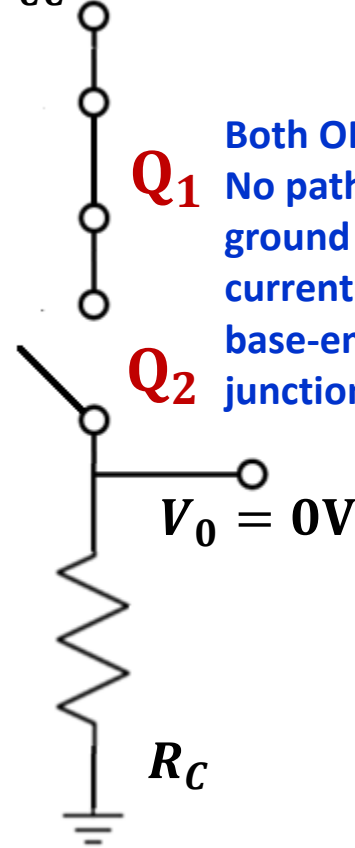
Base-emitter junction is conducting

$$0.4 \text{ mA}$$

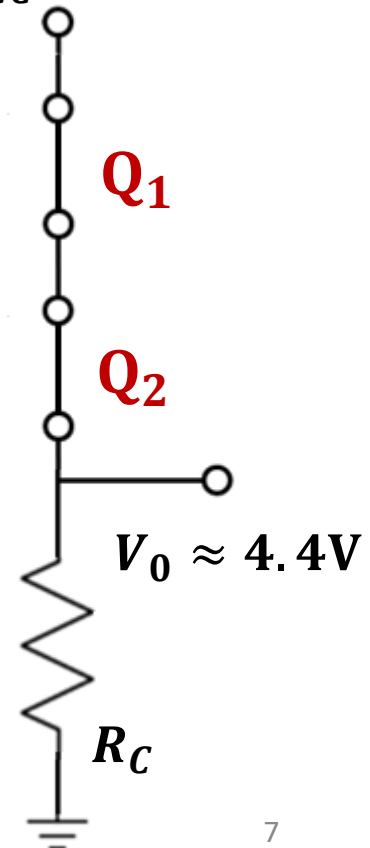


$$+V_{CC} = 5 \text{ V}$$

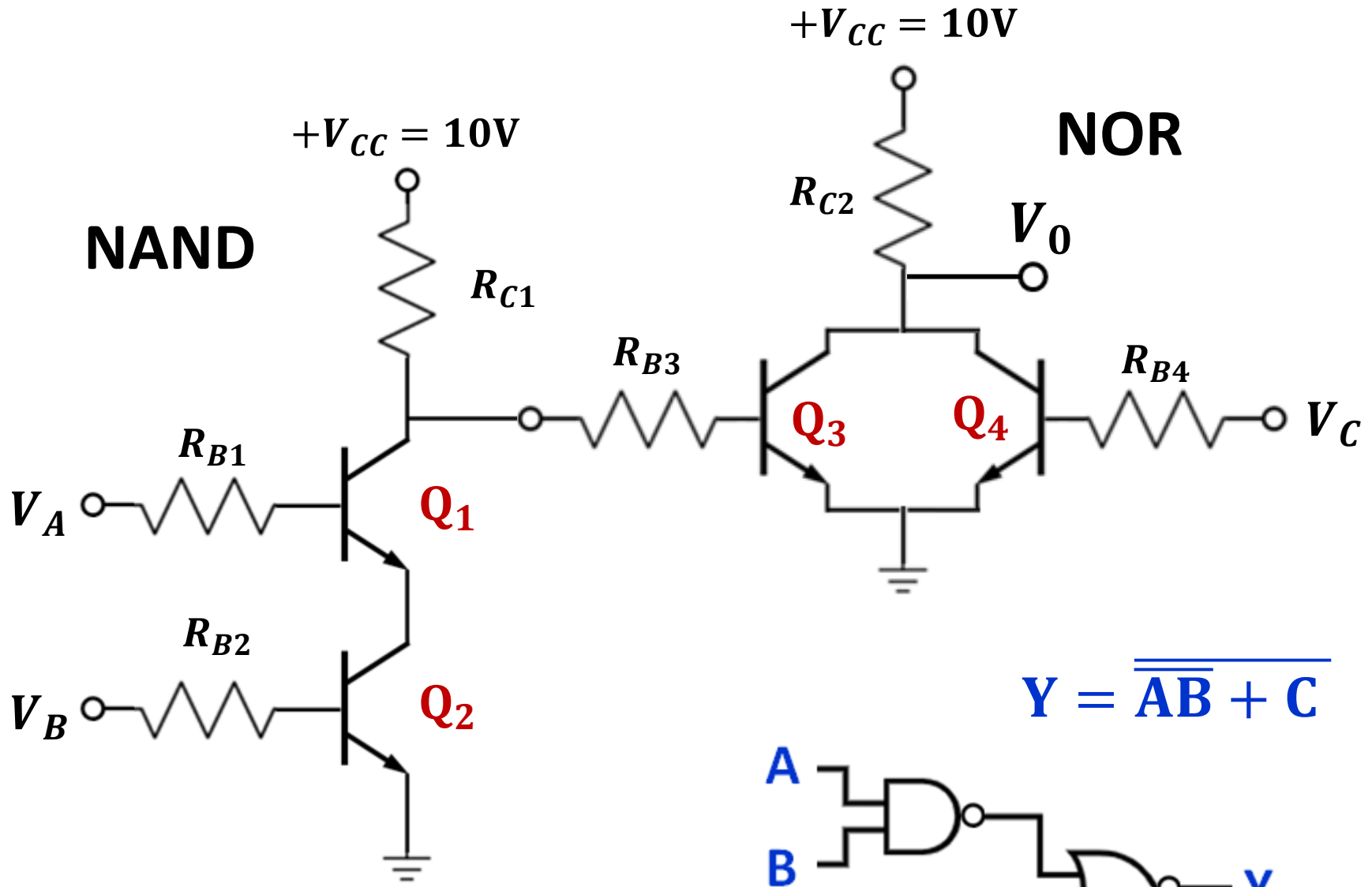
Both OFF
No path to ground for current in base-emitter junction of Q1



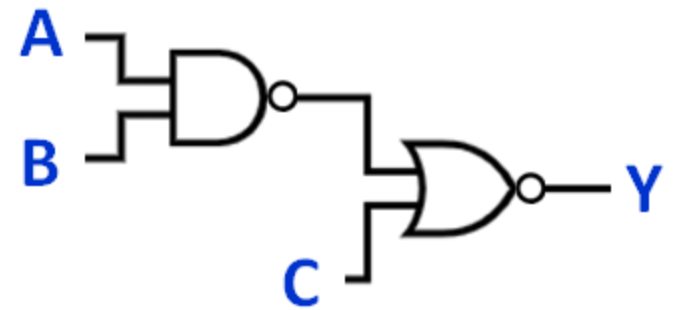
$$+V_{CC} = 5 \text{ V}$$

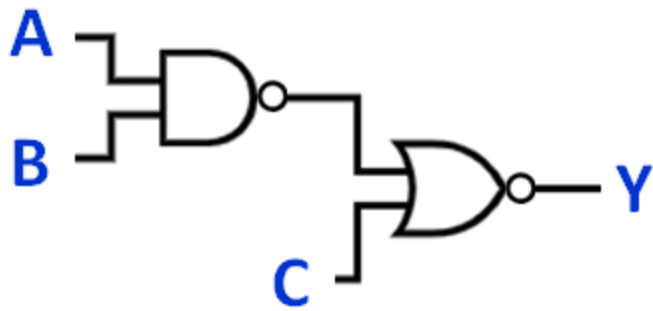


Another Example



$$Y = \overline{\overline{AB} + C}$$

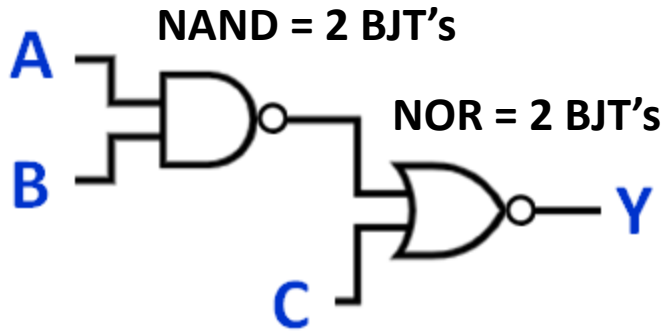




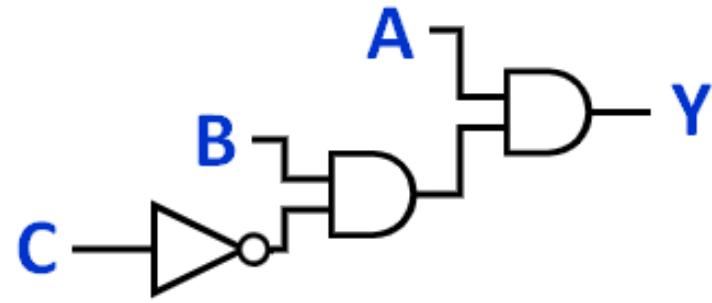
$$Y = \overline{\overline{AB}} + C$$

A	B	C	Y
0	0	0	0
0	0	1	0
0	1	0	0
0	1	1	0
1	0	0	0
1	0	1	0
1	1	0	1
1	1	1	0

What if we transform the circuit?



TOTAL = 4 BJT's



NOT = 1 BJT

Two 2-inputs NAND's = 4 BJT's

Two NOT's to obtain AND's = 2 BJT

TOTAL = 7 BJT's

$$Y = \overline{\overline{AB} + C}$$



Using De Morgan's theorem



$$Y = ABC\bar{C}$$

NOT = 1 BJT

One 3-inputs NAND = 3 BJT's

NOT to obtain AND = 1 BJT

TOTAL = 5 BJT's

Frequency response of circuits

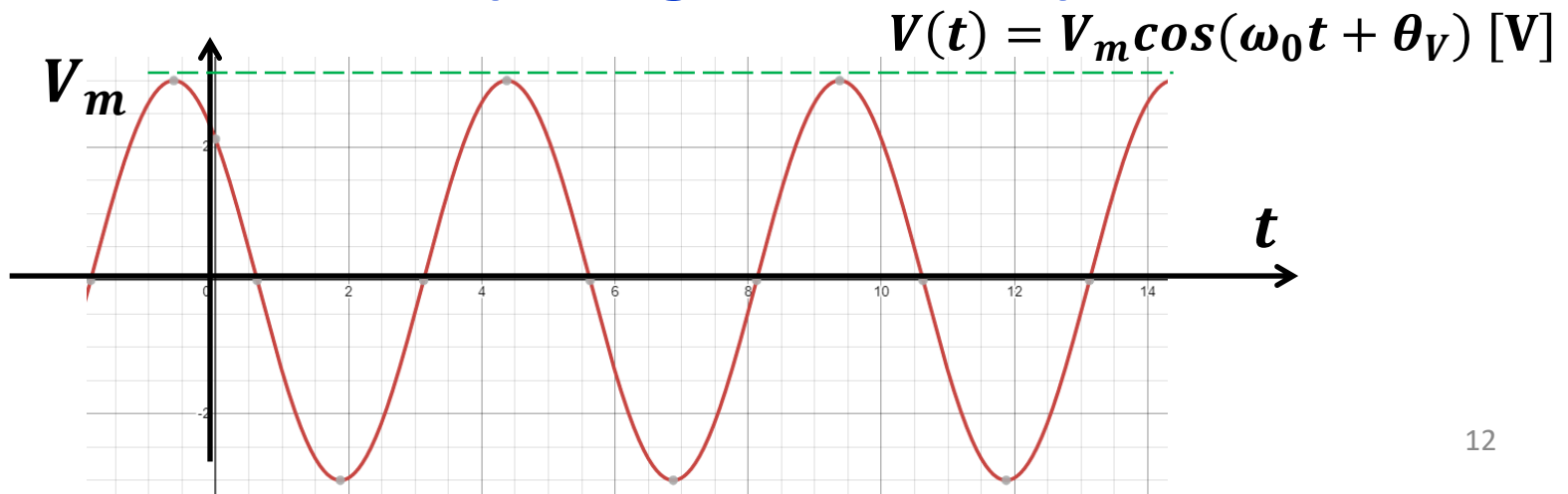
Frequency response

Until now we have considered the following forms of circuit excitation:

- **Constant source (voltage or current)**



- **Sinusoidal source (voltage or current)**



- **Constant source (voltage or current)**

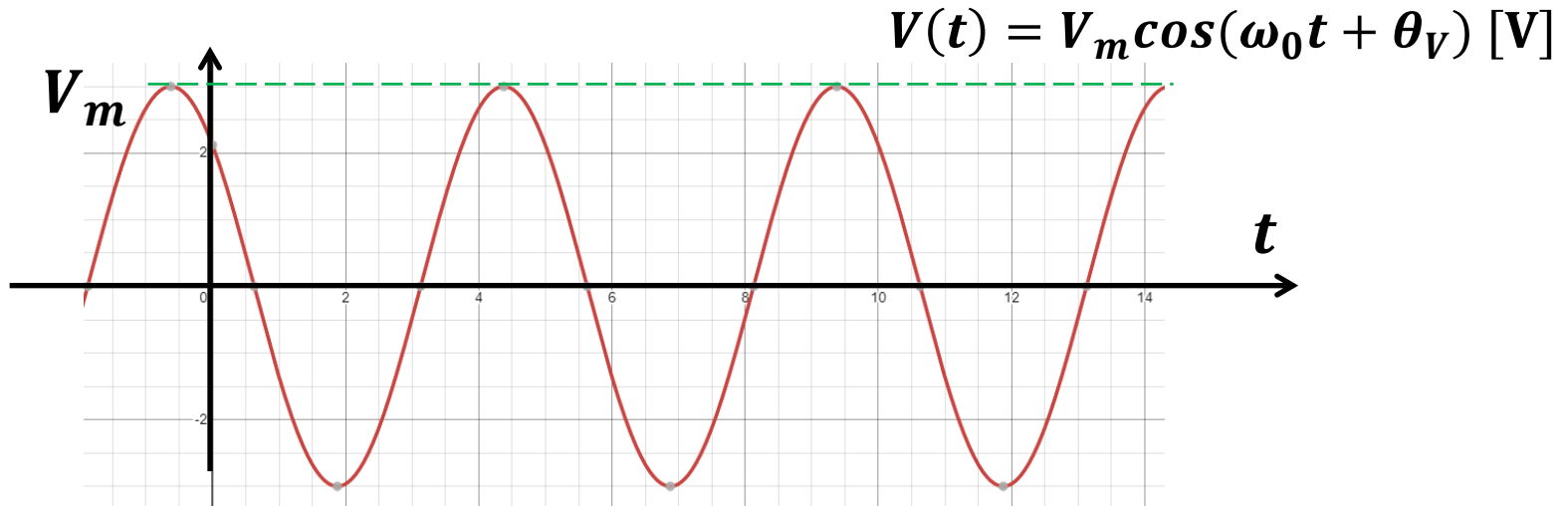


$$V(t) = K [V] = K \cos(0t)$$

$$\omega = 0 \text{ rad/s}$$

It can be interpreted as a signal with zero frequency

- Sinusoidal source (voltage or current)



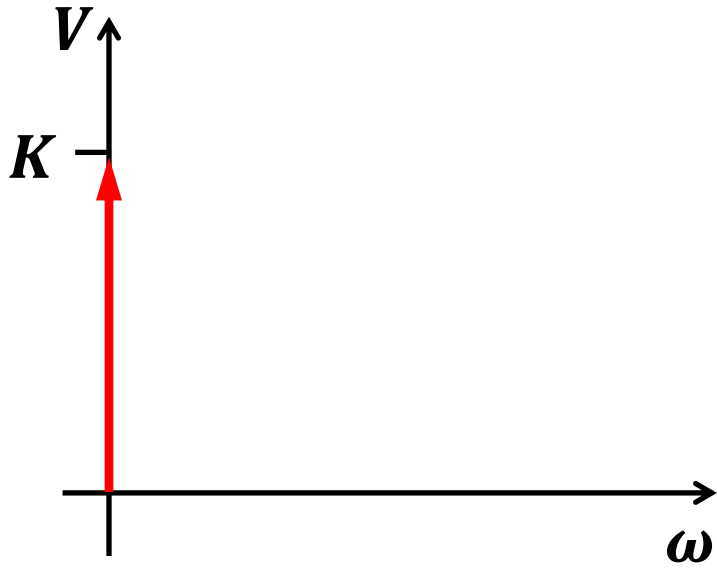
$$V(t) = V_m \cos(\omega_0 t + \theta_V)$$

$$\omega = 2\pi f_0 \text{ rad/s}$$

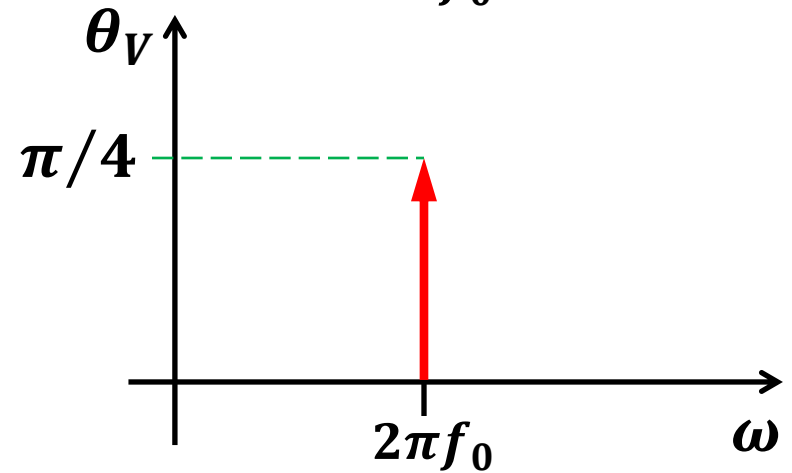
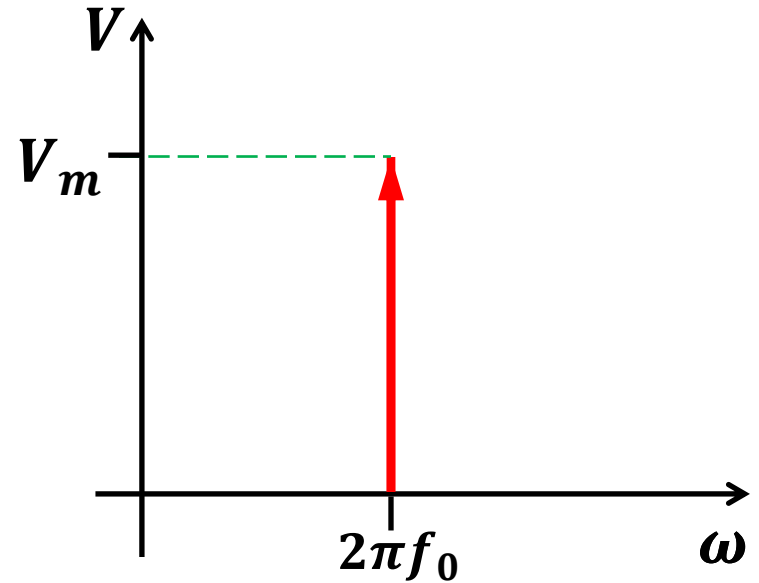
$$\theta_V = \frac{\pi}{4} \text{ rad}$$

This is a signal with a single frequency component f_0

Representation in the frequency domain



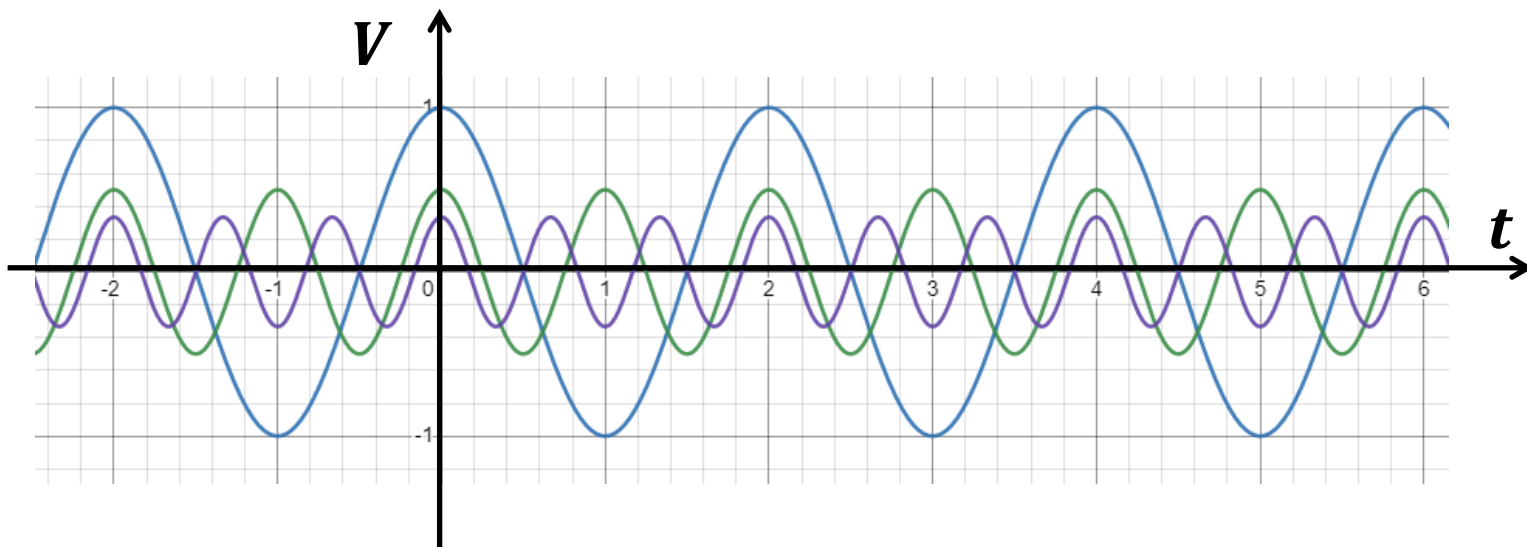
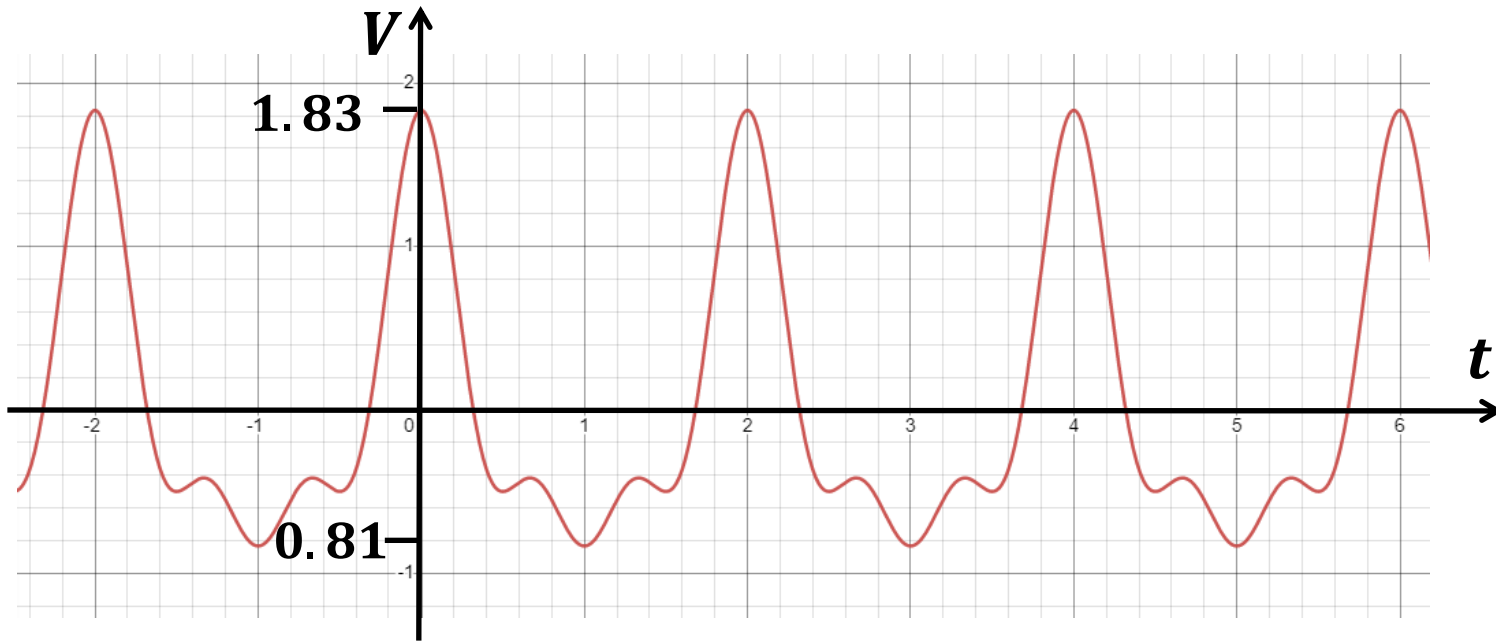
$$V(t) = K$$



$$V(t) = V_m \cos(\omega_0 t + \pi/4)$$

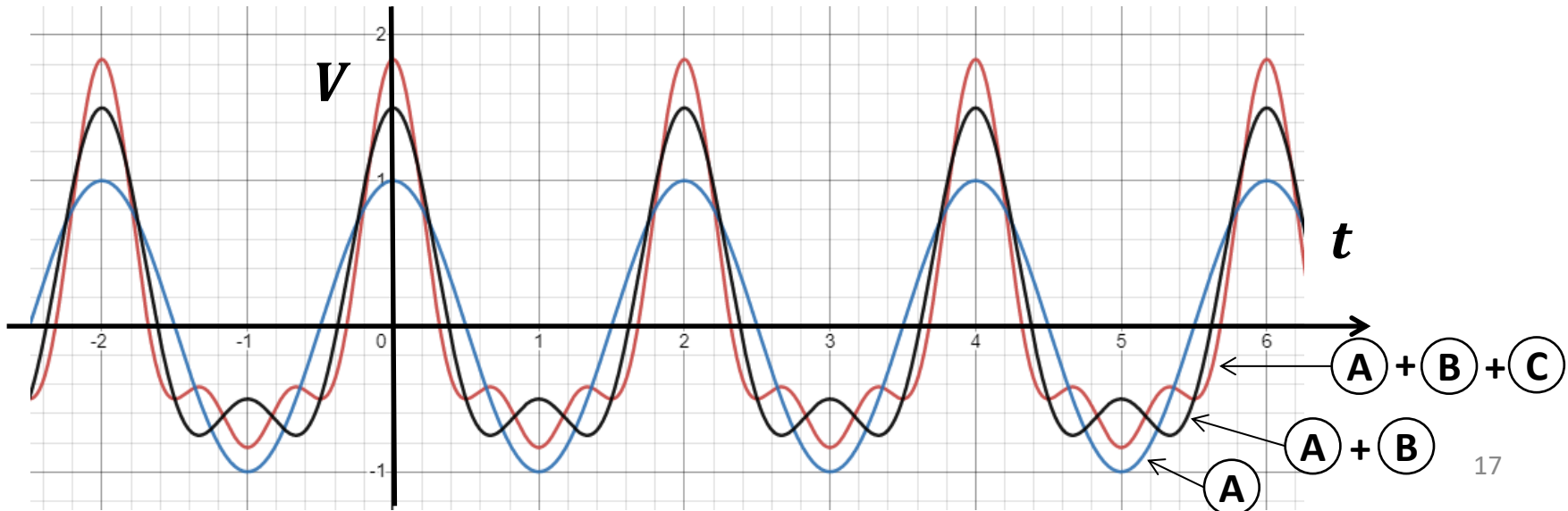
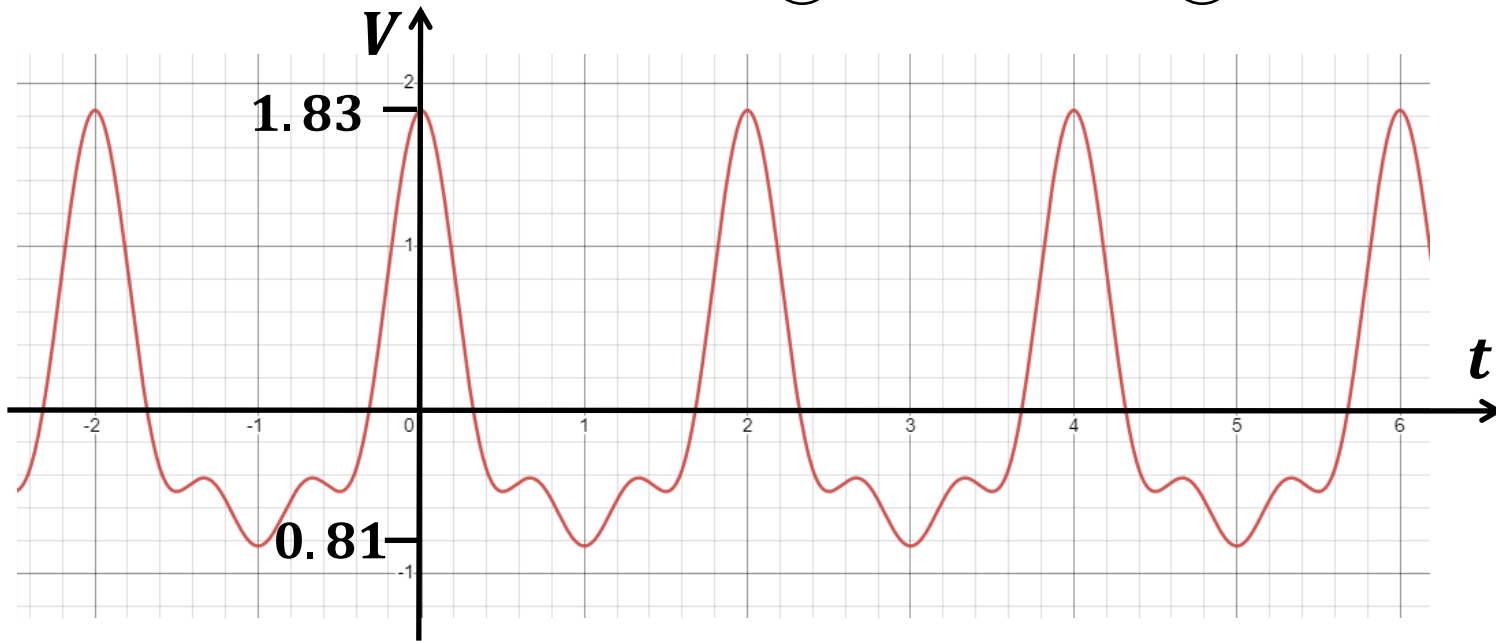
Signal with several frequencies

$$V(t) = \cos(\omega_0 t) + \frac{1}{2} \cos(2\omega_0 t) + \frac{1}{3} \cos(3\omega_0 t)$$



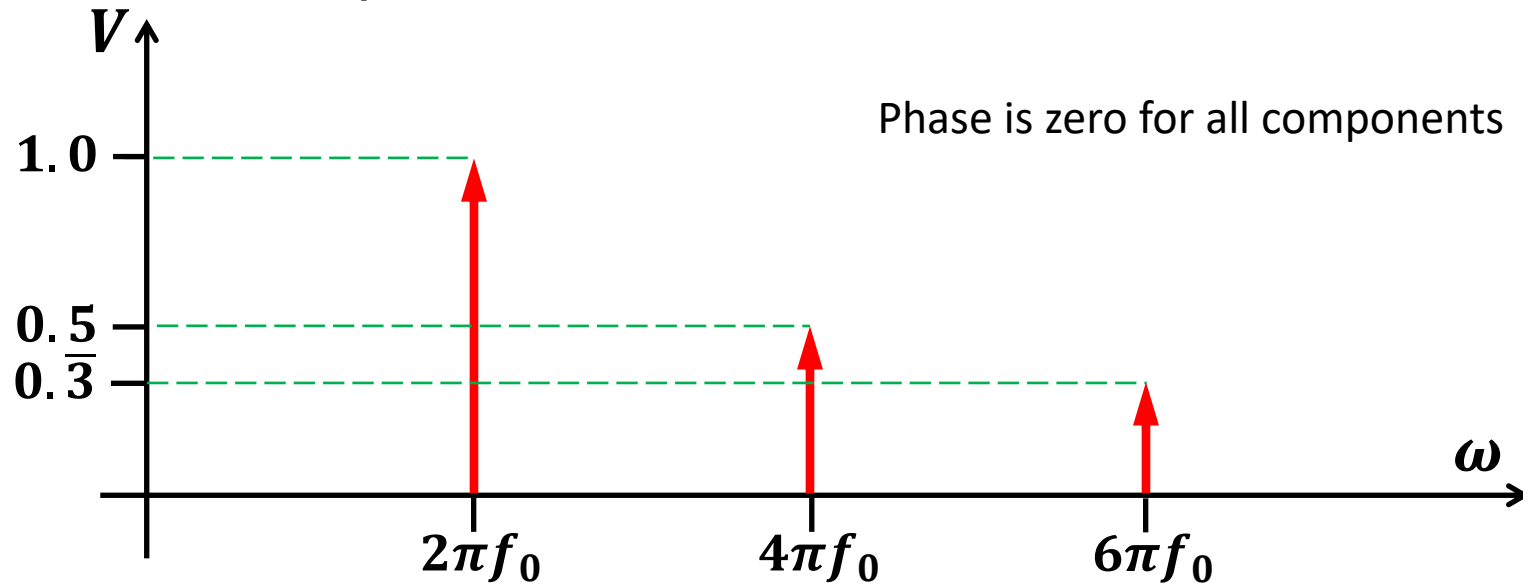
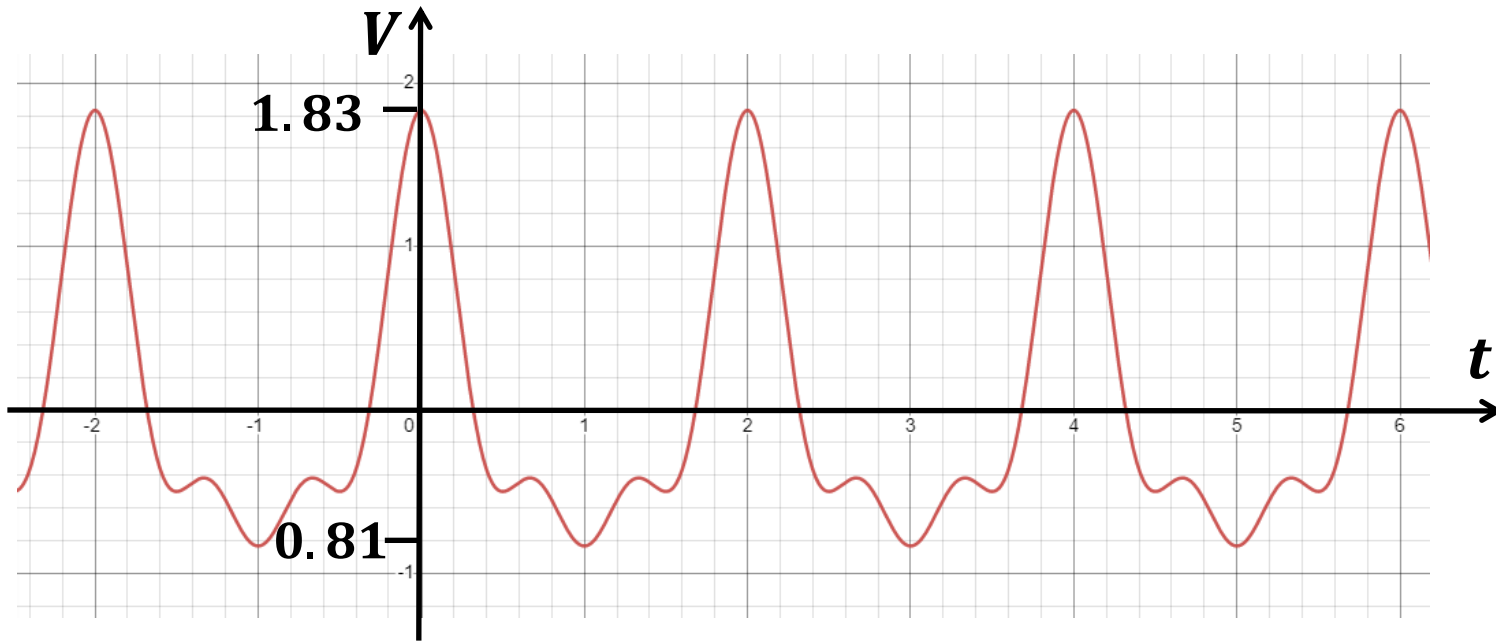
Signal with several frequencies

$$V(t) = \underbrace{\cos(\omega_0 t)}_{\text{A}} + \underbrace{\frac{1}{2} \cos(2\omega_0 t)}_{\text{B}} + \underbrace{\frac{1}{3} \cos(3\omega_0 t)}_{\text{C}}$$

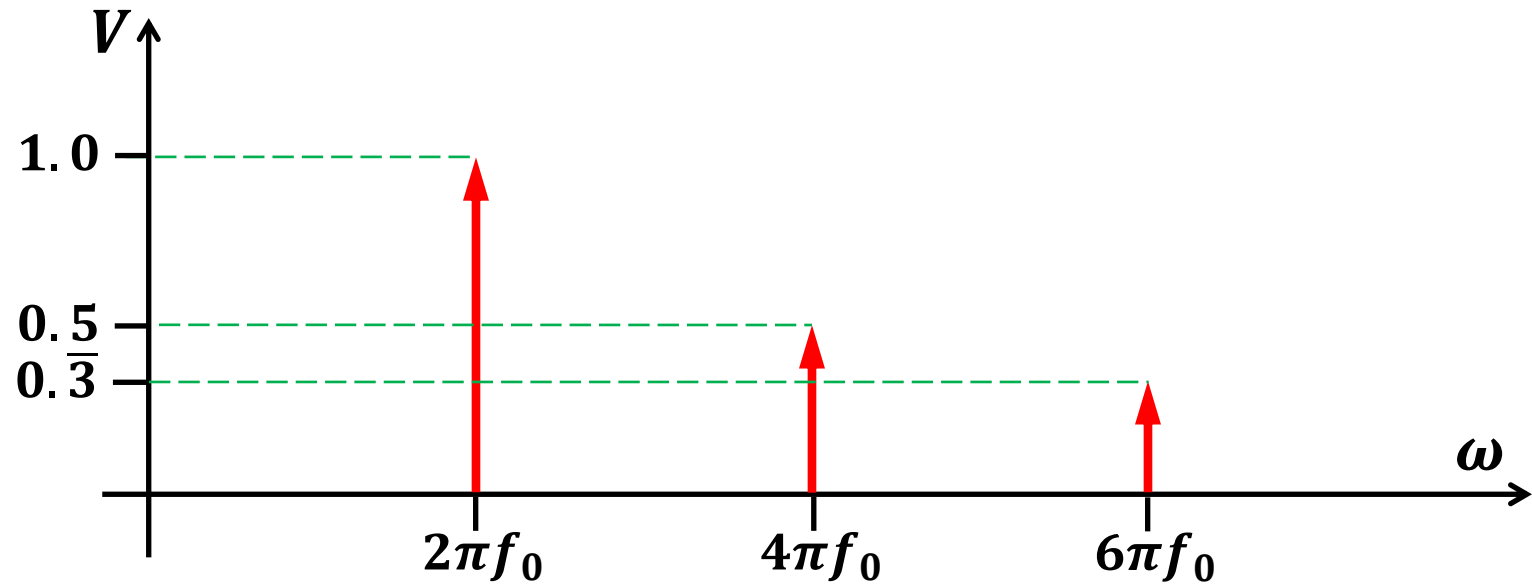
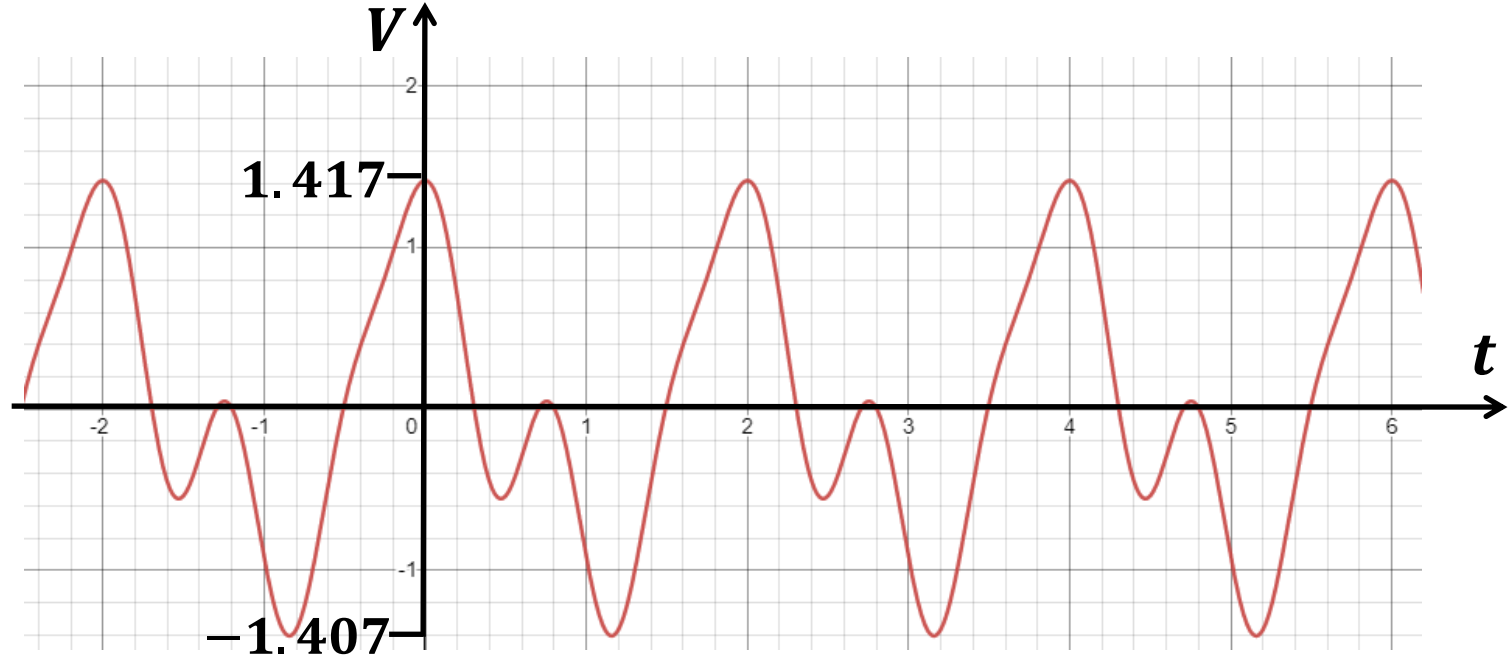


Signal with several frequencies

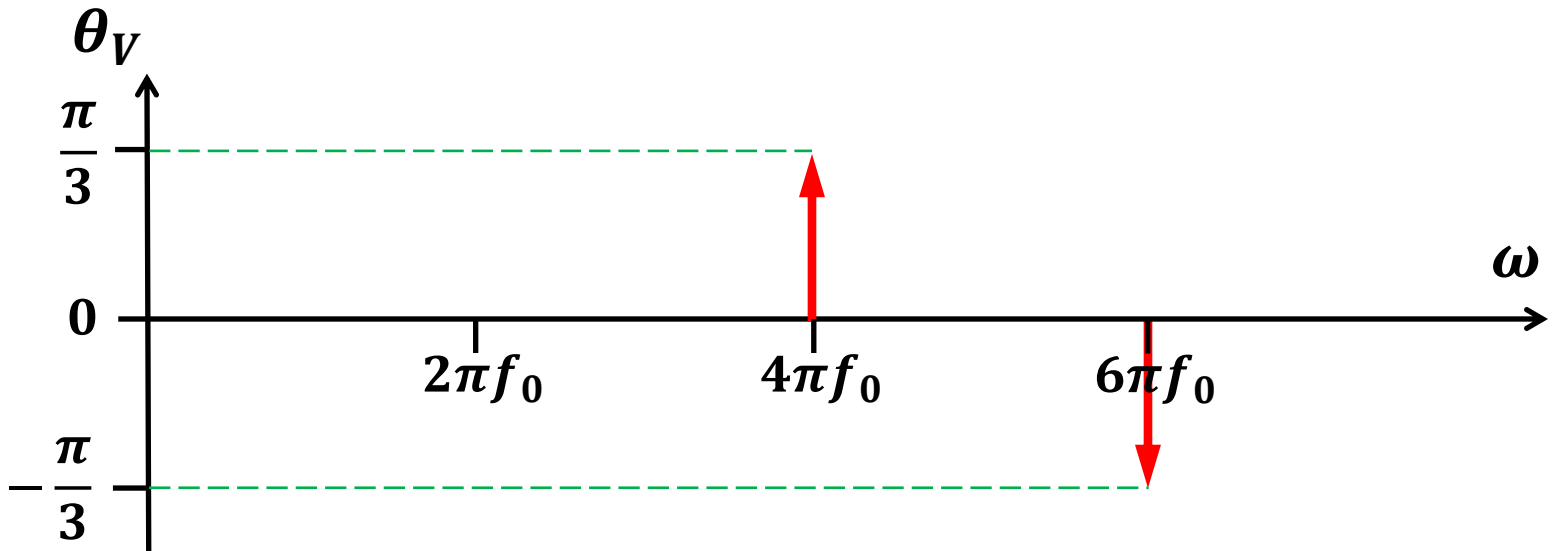
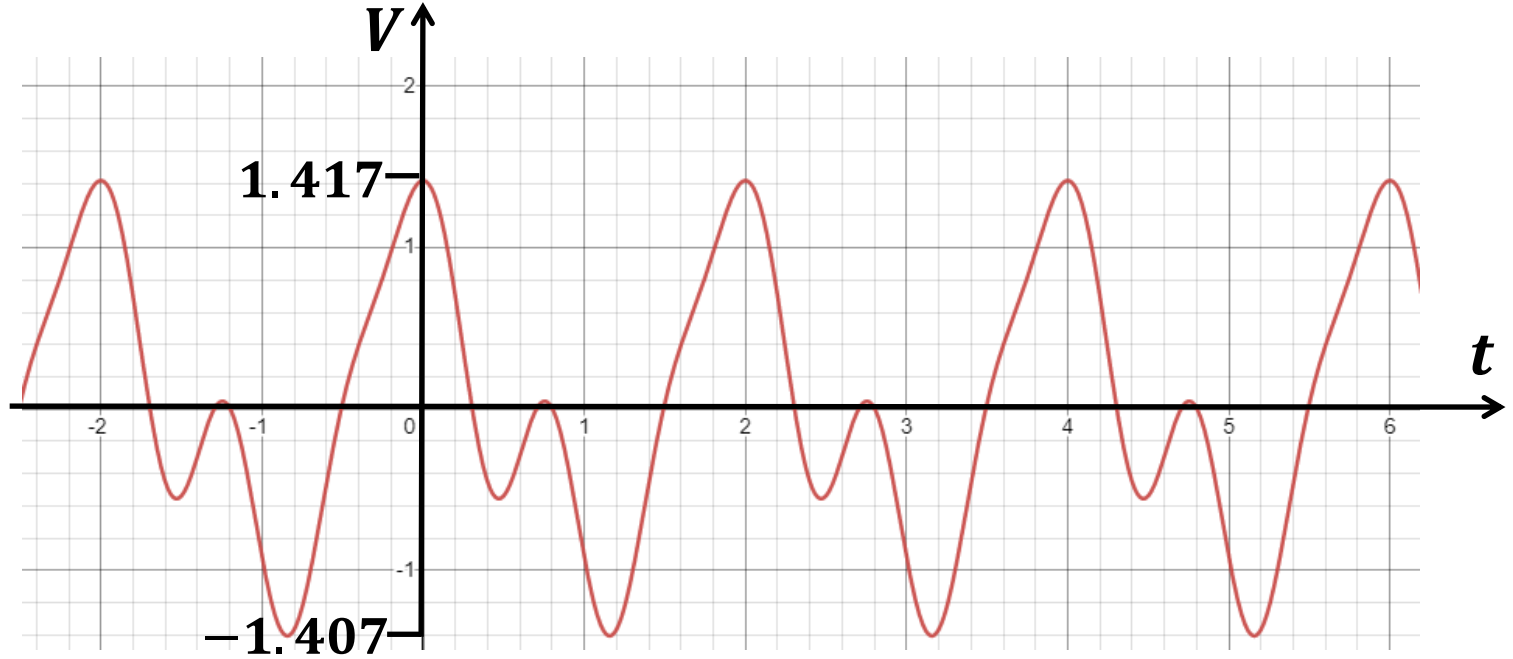
$$V(t) = \cos(\omega_0 t) + \frac{1}{2} \cos(2\omega_0 t) + \frac{1}{3} \cos(3\omega_0 t)$$



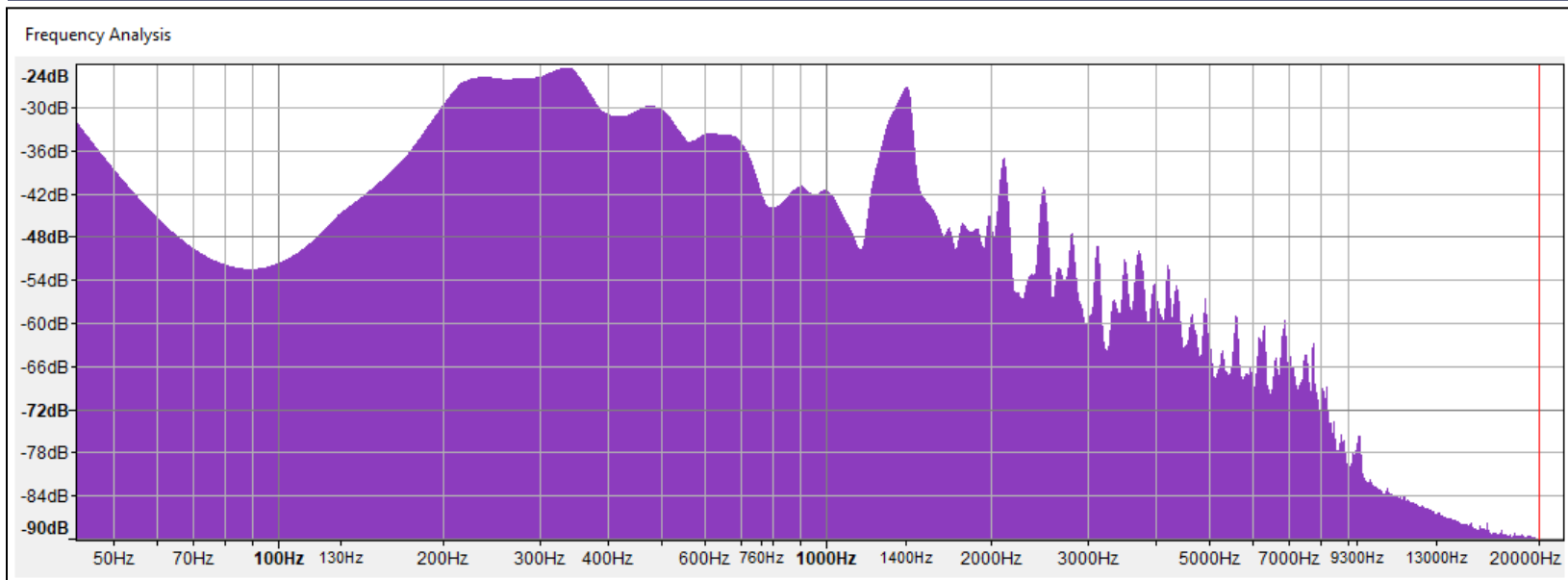
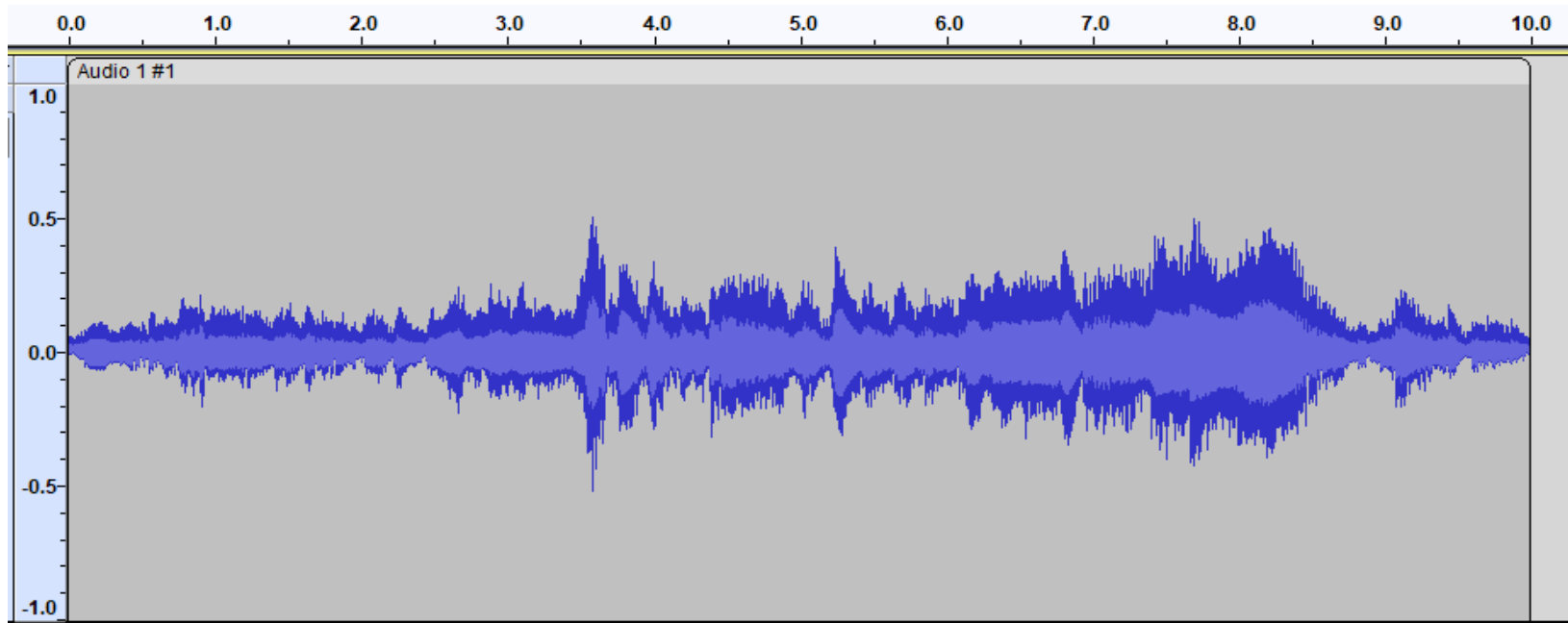
$$V(t) = \cos(\omega_0 t) + \frac{1}{2} \cos\left(2\omega_0 t + \frac{\pi}{3}\right) + \frac{1}{3} \cos\left(3\omega_0 t - \frac{\pi}{3}\right)$$



$$V(t) = \cos(\omega_0 t) + \frac{1}{2} \cos\left(2\omega_0 t + \frac{\pi}{3}\right) + \frac{1}{3} \cos\left(3\omega_0 t - \frac{\pi}{3}\right)$$



Ten seconds of music and its frequency "spectrum"



Excerpt from: Dmitri Shostakovich, Concerto No.1 for piano, trumpet and strings in C minor, Op. 35 (ORFEO - C220011)

Fourier transform

Converts a time domain signal $V(t)$ to a frequency domain signal $\tilde{V}(\omega)$

$$\tilde{V}(\omega) = \int_{-\infty}^{\infty} V(t) e^{-j\omega t} dt$$

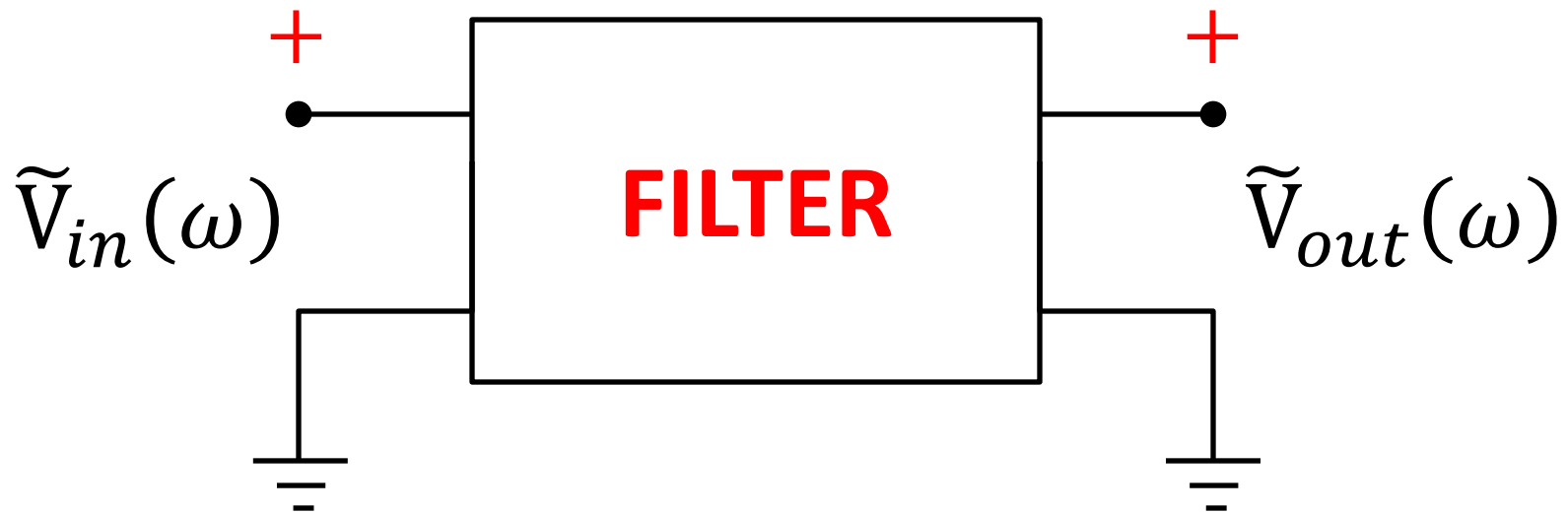
In general, the Fourier Transform is a complex function

Anti-Transform

$$V(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \tilde{V}(\omega) e^{j\omega t} d\omega$$

Filter

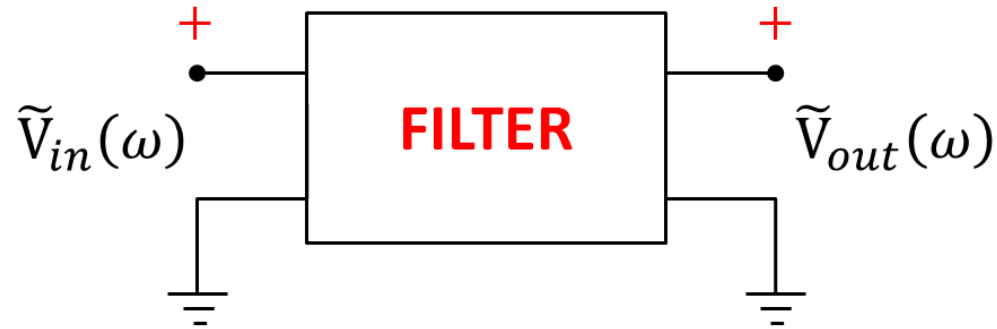
A circuit which manipulates a signal, typically by changing the relative amplitudes of the frequency components.



We will consider filters (systems) which are “single-input” and “single-output,” consisting of “linear” and “time-invariant” circuits.

Transfer Function

The relationship linking the frequency-dependent input and output



$$\tilde{V}_{out}(\omega) = \mathbf{H}(\omega) \tilde{V}_{in}(\omega)$$

$$\mathbf{H}(\omega) = \frac{\tilde{V}_{out}(\omega)}{\tilde{V}_{in}(\omega)} = |\mathbf{H}(\omega)| \angle \theta(\omega)$$

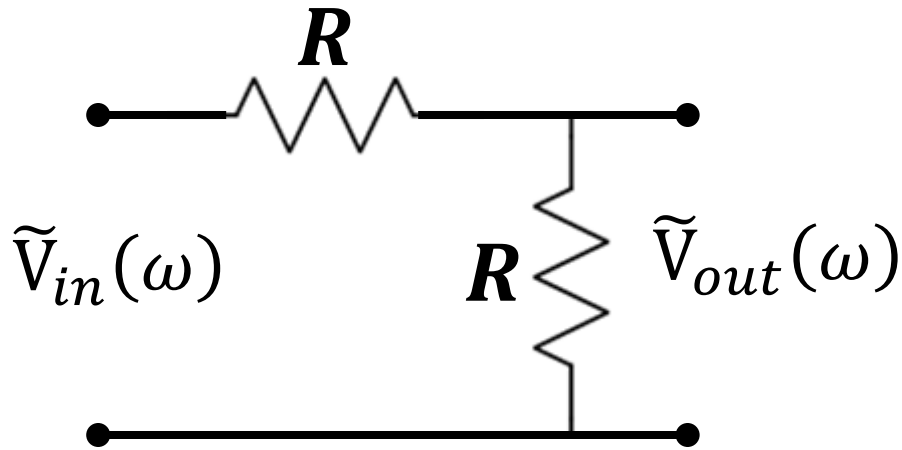
Transfer
Function

Magnitude
Response

Phase
Response

1 – Voltage Divider

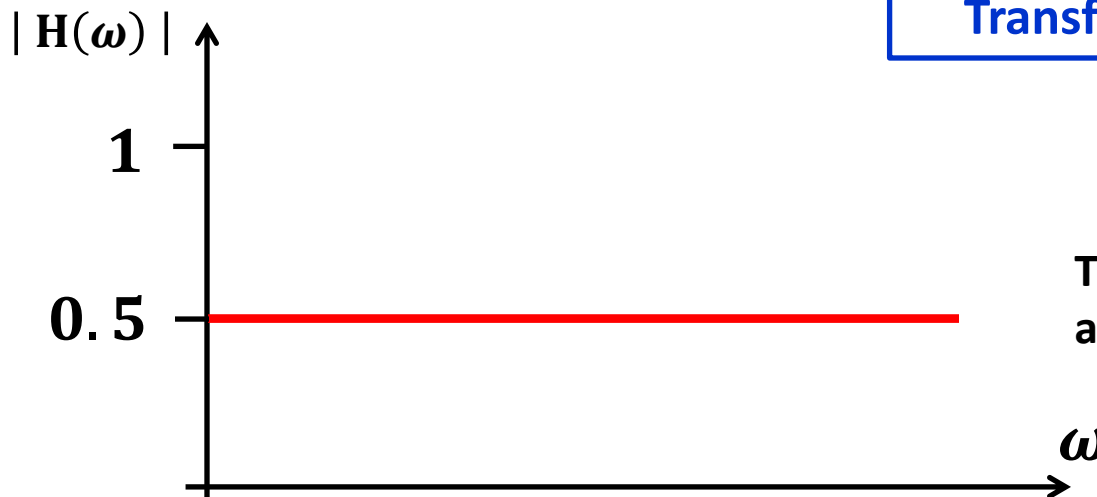
The voltage divider is a very simple filter



$$\tilde{V}_{out}(\omega) = \frac{1}{2} \tilde{V}_{in}(\omega)$$

$$\mathbf{H}(\omega) = |\mathbf{H}(\omega)| = \frac{1}{2}$$

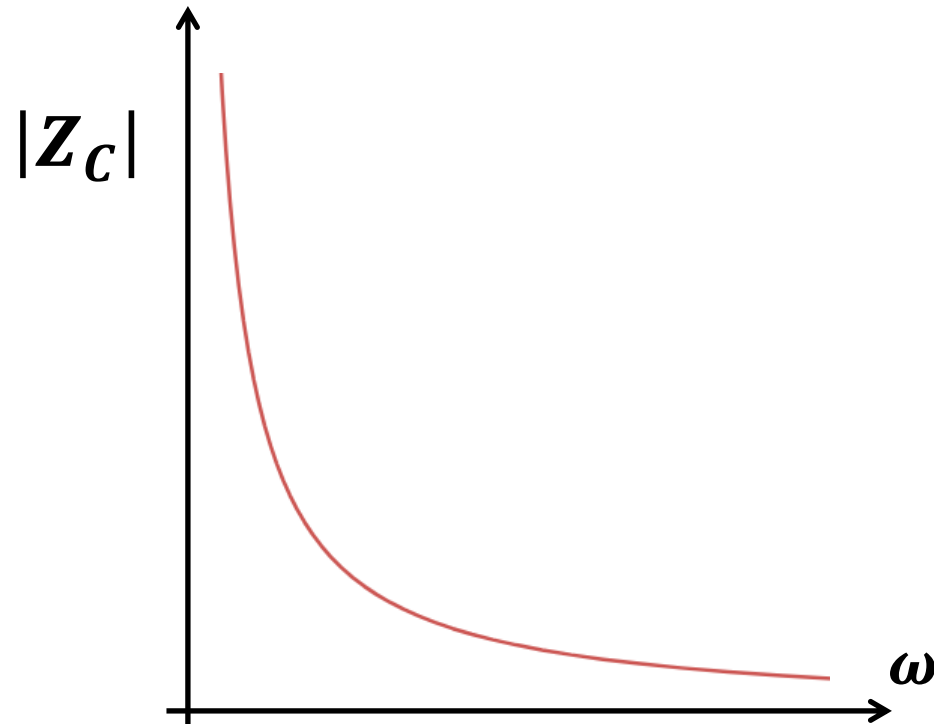
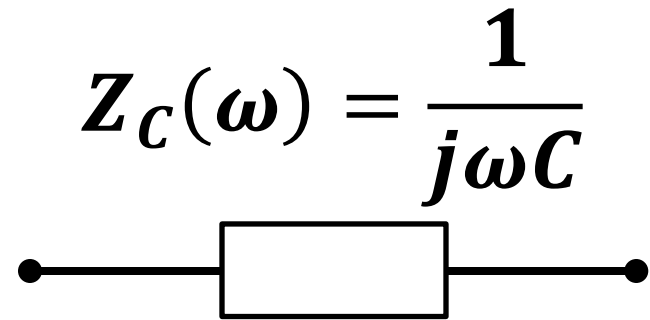
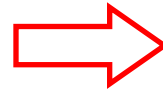
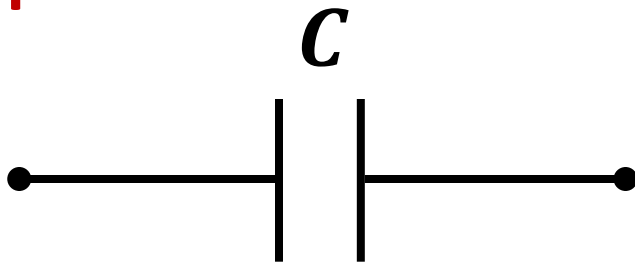
Transfer Function



This circuit works as an “attenuator”

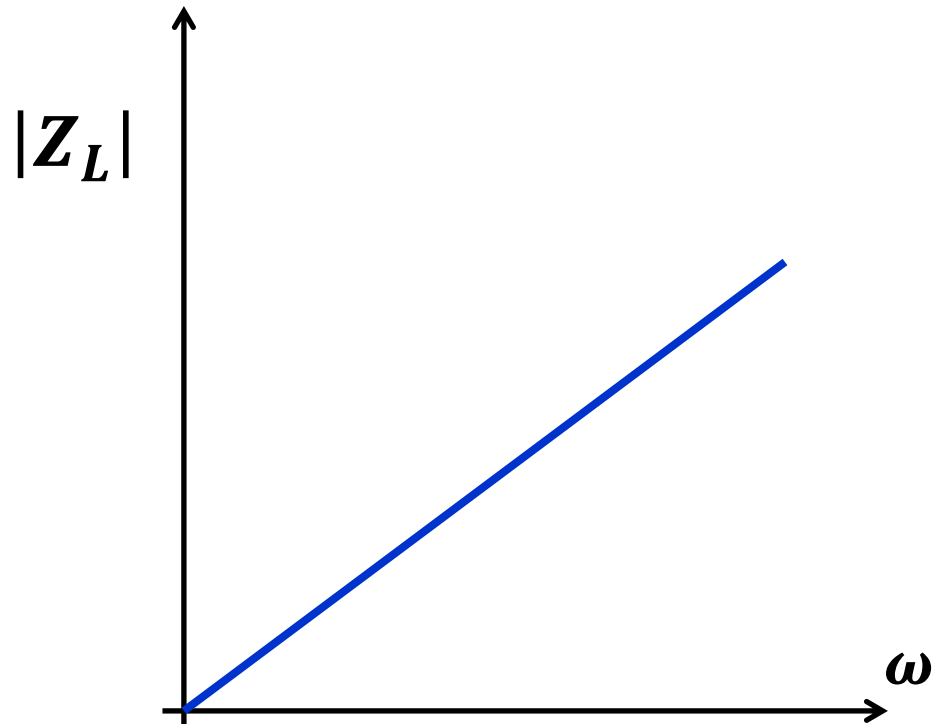
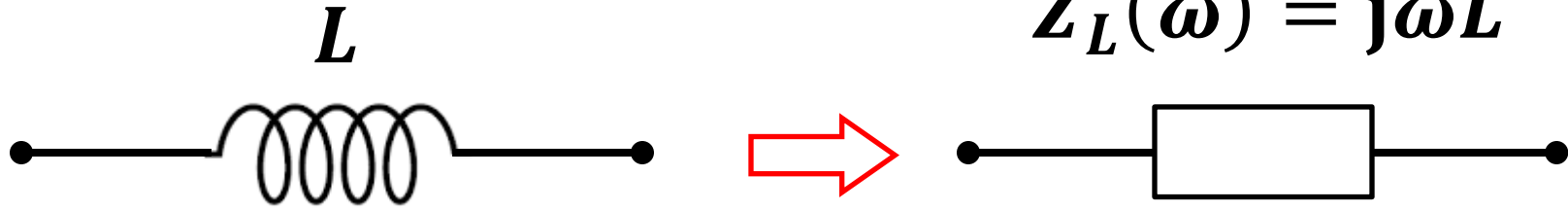
Behavior of Reactive Circuit Elements

Capacitor



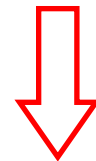
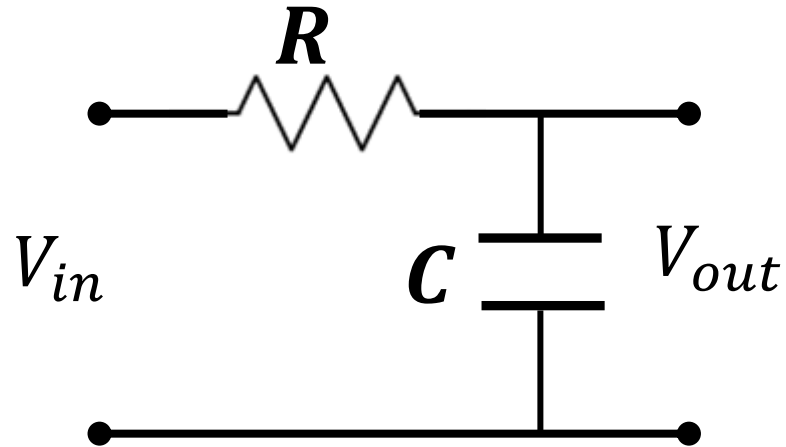
Behavior of Reactive Circuit Elements

Inductor

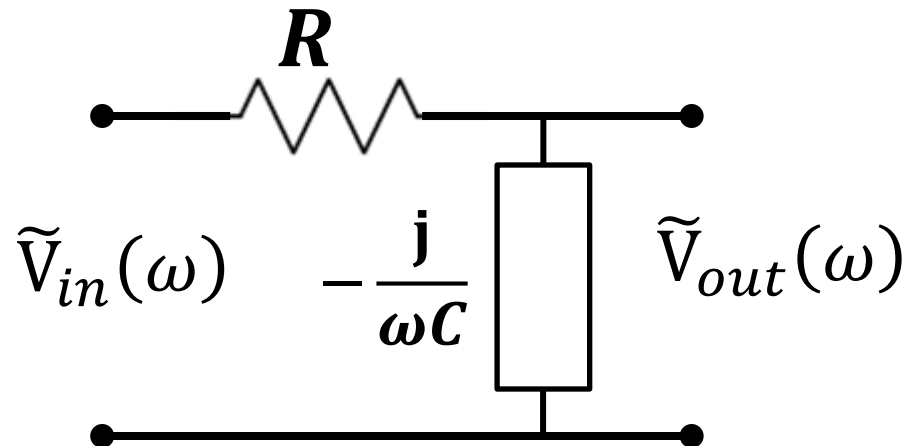


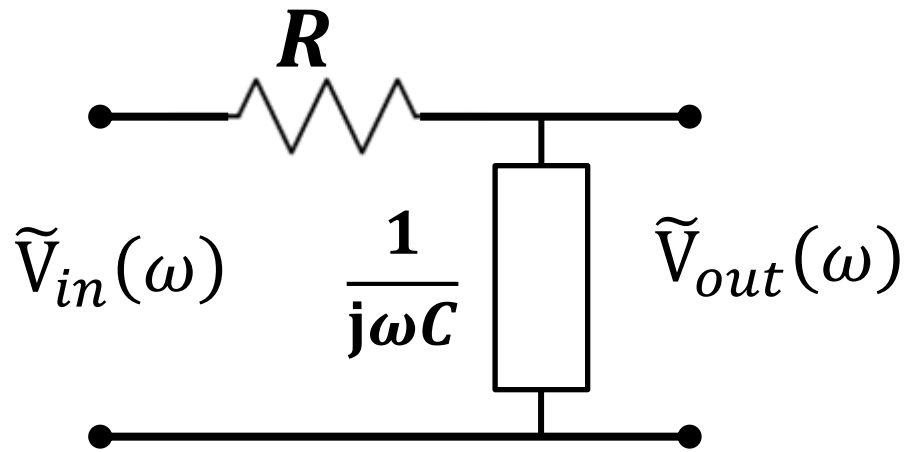
2 – Low Pass RC filter

RC filter
(1st order)



PHASORS





Let the input be a phasor of the form

$$\tilde{V}_{in}(\omega) = V_I \angle 0^\circ$$

$$\tilde{V}_{out}(\omega) = V_I \angle 0^\circ \frac{1/j\omega C}{R + 1/j\omega C} = \overbrace{V_I \angle 0^\circ}^{\tilde{V}_{in}(\omega)} \frac{1}{1 + j\omega RC}$$

$$\frac{\tilde{V}_{out}(\omega)}{\tilde{V}_{in}(\omega)} = \mathbf{H}(\omega) = \frac{1}{1 + j\omega RC}$$

Transfer Function

$$\mathbf{H(\omega) = \frac{1}{1 + j\omega RC}}$$

$$\mathbf{H(\omega) = \frac{1 - j\omega RC}{(1 + j\omega RC)(1 - j\omega RC)} = \frac{1 - j\omega RC}{1 + (\omega RC)^2}}$$

Cartesian Form

Magnitude

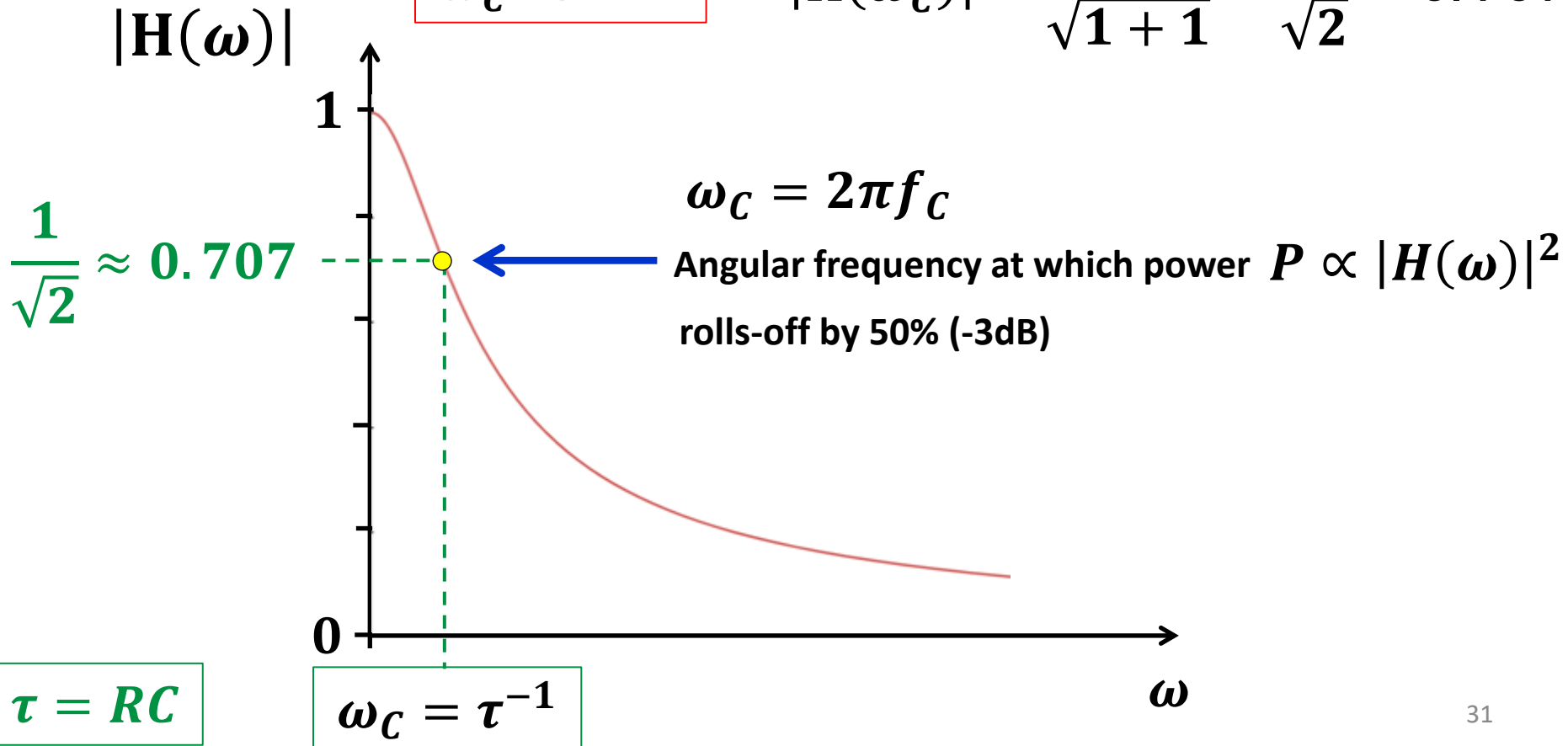
$$|\mathbf{H(\omega)}| = \frac{1}{|1 + j\omega RC|}$$

$$|\mathbf{H(\omega)}| = \frac{1}{\sqrt{1 + (\omega RC)^2}}$$

Magnitude of $H(\omega)$ for RC low-pass filter

$$|H(\omega)| = \frac{1}{\sqrt{1 + (\omega RC)^2}}$$

$$\omega_c RC = 1 \rightarrow |H(\omega_c)| = \frac{1}{\sqrt{1 + 1}} = \frac{1}{\sqrt{2}} = 0.707$$

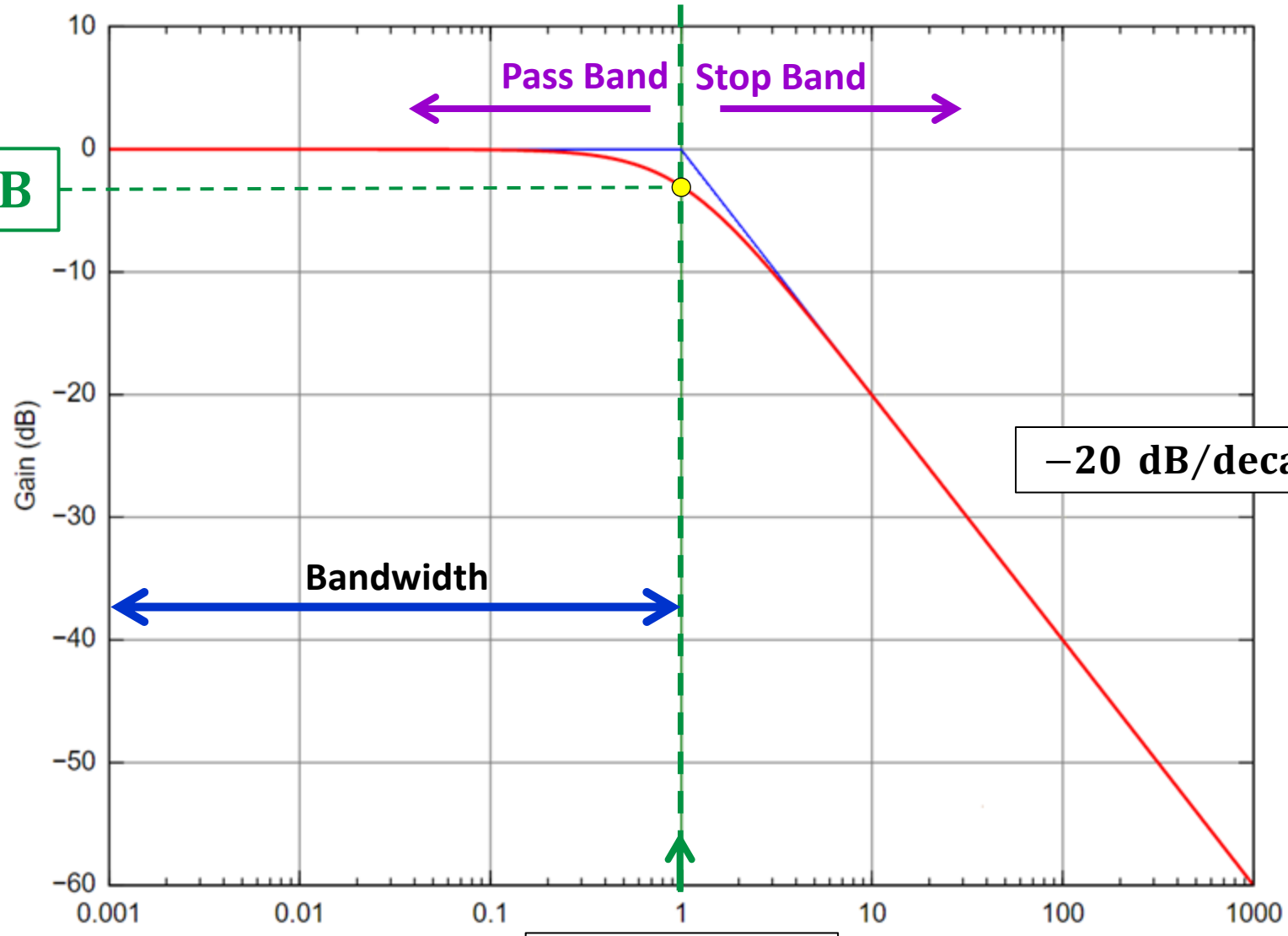


log-decibel representation – Bode Plot for magnitude

$$20 \log_{10} \left(\frac{V_{out}}{V_{in}} \right)$$

NOTE: This plot is normalized so that $\omega_c = 1$

-3dB



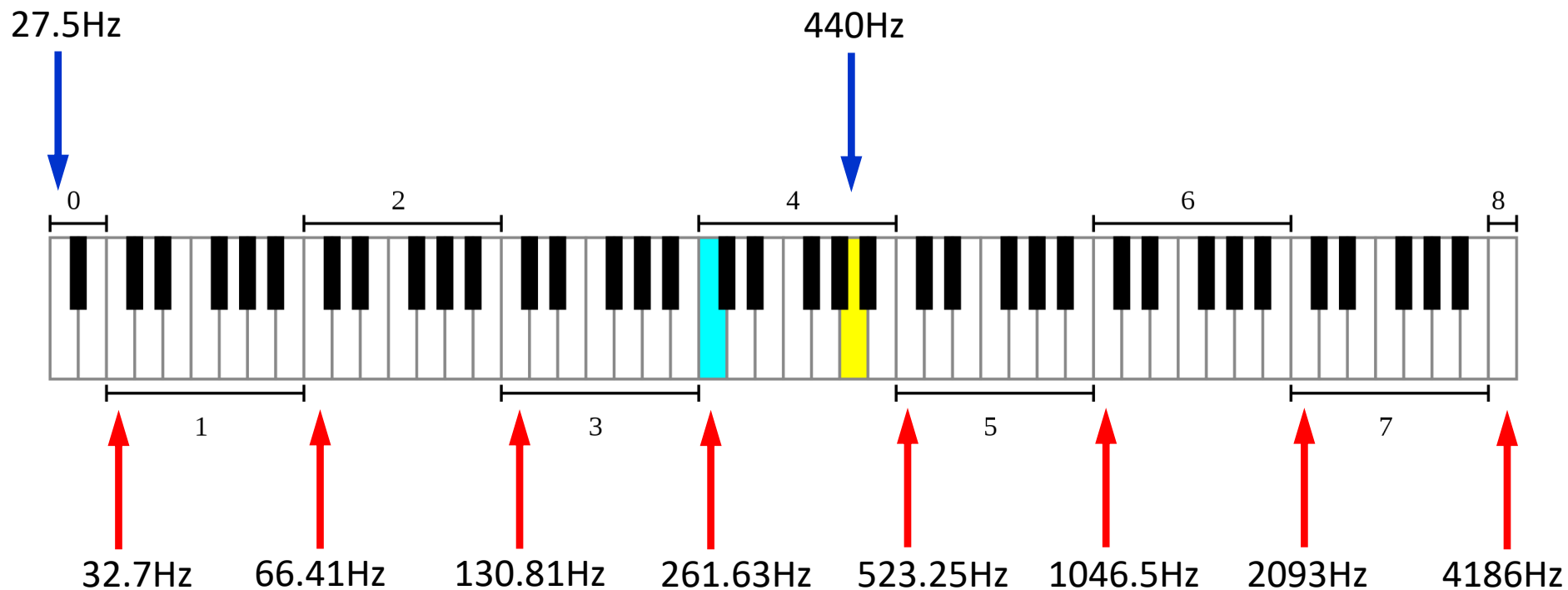
Cut-off frequency

$$\omega_c = 2\pi f_c$$

-20 dB/decade

ω [rad/s]

The piano keyboard uses octaves (instead of decades)



Phase of $H(\omega)$ for RC low-pass filter

$$H(\omega) = \frac{1 - j\omega RC}{(1 + j\omega RC)(1 - j\omega RC)} = \frac{1 - j\omega RC}{\underbrace{1 + (\omega RC)^2}_{\text{Cartesian Form}}}$$

$$\angle H(\omega) = \tan^{-1} \frac{\Im\{H(\omega)\}}{\Re\{H(\omega)\}} = \tan^{-1} \frac{-\omega RC / (1 + (\omega RC)^2)}{1 / (1 + (\omega RC)^2)}$$

$$\angle H(\omega) = \tan^{-1}(-\omega RC) = -\tan^{-1}(\omega RC)$$

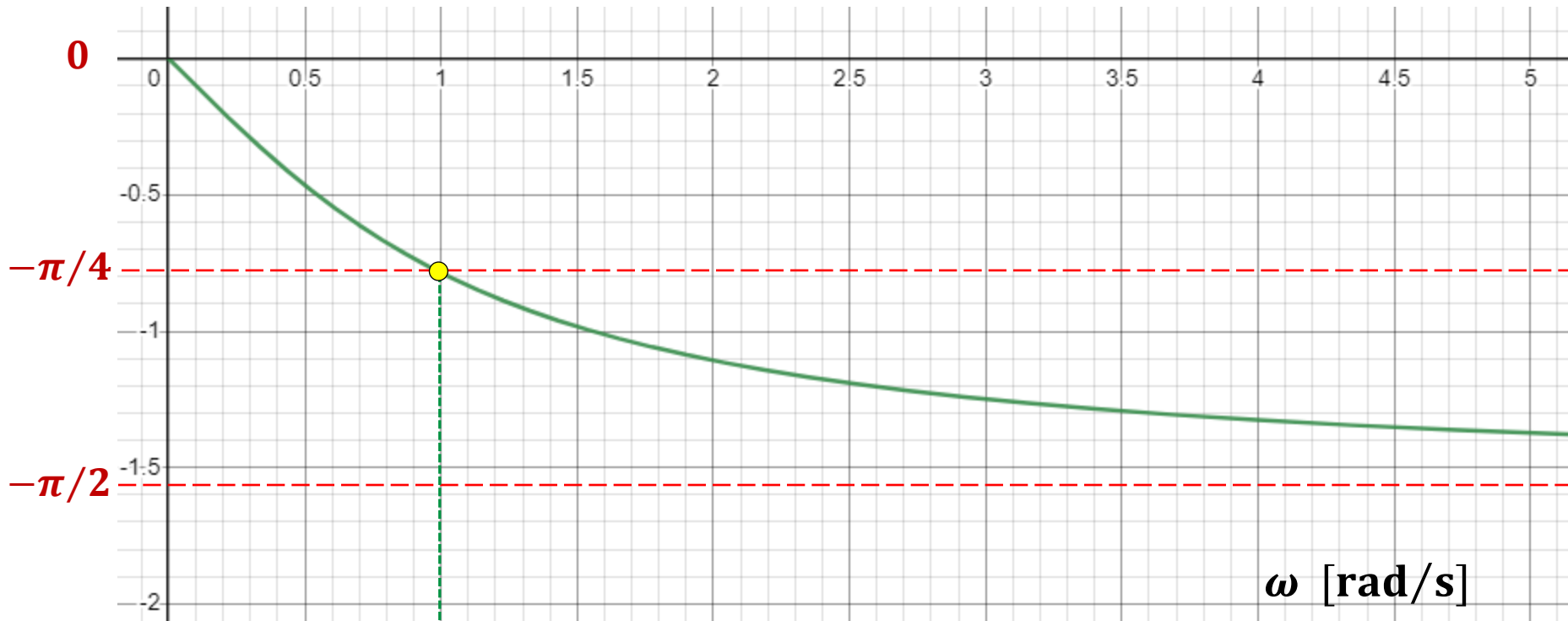
When $\omega = \omega_c$ we have $\omega_c RC = 1$

$$\angle H(\omega) = \tan^{-1}(-1) = -\frac{\pi}{4} = -45^\circ$$

Phase for RC low-pass filter

Linear scale representation

$\angle H(\omega)$ [rad]



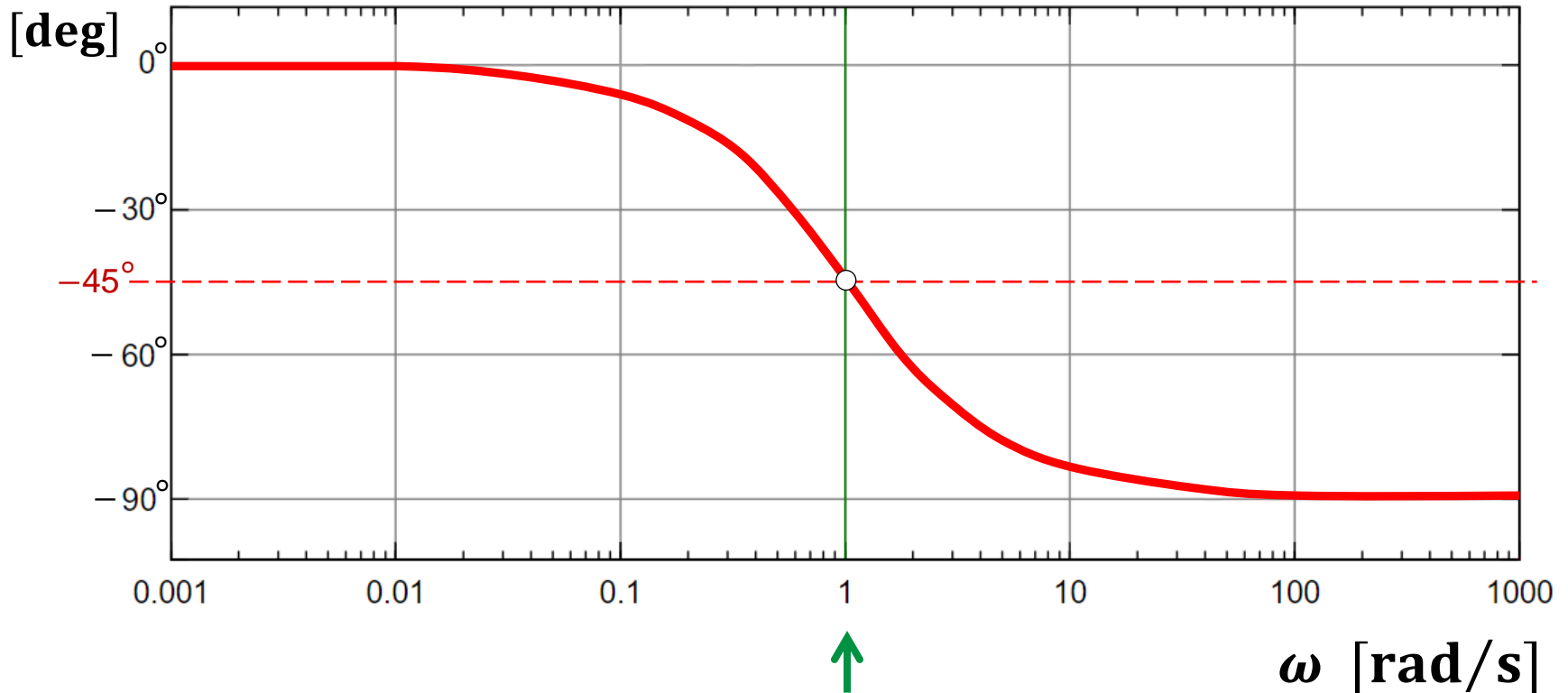
$$\omega_c = 2\pi f_c$$

Phase for RC low-pass filter

semi-log scale representation – Bode Plot for phase

NOTE: This plot is normalized so that $\omega_C = 1$

$\angle H(\omega)$



$$\omega_C = 2\pi f_C$$

Example - RC low-pass filter

ω_1

Consider $R = 2.5 \text{ k}\Omega$ and $C = 400 \text{ nF}$

$$\omega_0 = 1/(RC) = (2.5\text{k} \times 400 \times 10^{-9})^{-1} = 10^3 \text{ rad/s}$$

$$f = 60\text{Hz}$$

$$\omega_1 \approx 377 \text{ rad/s}$$

$$\omega_1 RC = 2\pi \times 60 \times 2.5\text{k} \times 400 \times 10^{-9} \approx 377.0$$

$$|H(\omega_1)| = \frac{1}{\sqrt{1 + (\omega_1 RC)^2}} = 0.9357$$

$$|H(\omega_1)|_{\text{dB}} = 20 \log_{10}(0.9357) = -0.5772 \text{ dB}$$

Example - RC low-pass filter

ω_2

Consider $R = 2.5 \text{ k}\Omega$ and $C = 400 \text{ nF}$

$$\omega_0 = 1/(RC) = (2.5\text{k} \times 400 \times 10^{-9})^{-1} = 10^3 \text{ rad/s}$$

$$f = 160\text{Hz}$$

$$\omega_2 = 1005.3 \text{ rad/s}$$

$$\omega_2 RC = 2\pi \times 160 \times 2.5\text{k} \times 400 \times 10^{-9} \approx 1.0$$

$$|H(\omega_2)| = \frac{1}{\sqrt{1 + (\omega_2 RC)^2}} = 0.7052$$

$$|H(\omega_2)|_{\text{dB}} = 20 \log_{10}(0.7052) = -3.033 \text{ dB}$$

Example - RC low-pass filter

ω_3

Consider $R = 2.5 \text{ k}\Omega$ and $C = 400 \text{ nF}$

$$\omega_0 = 1/(RC) = (2.5\text{k} \times 400 \times 10^{-9})^{-1} = 10^3 \text{ rad/s}$$

$$f = 16 \text{ kHz}$$

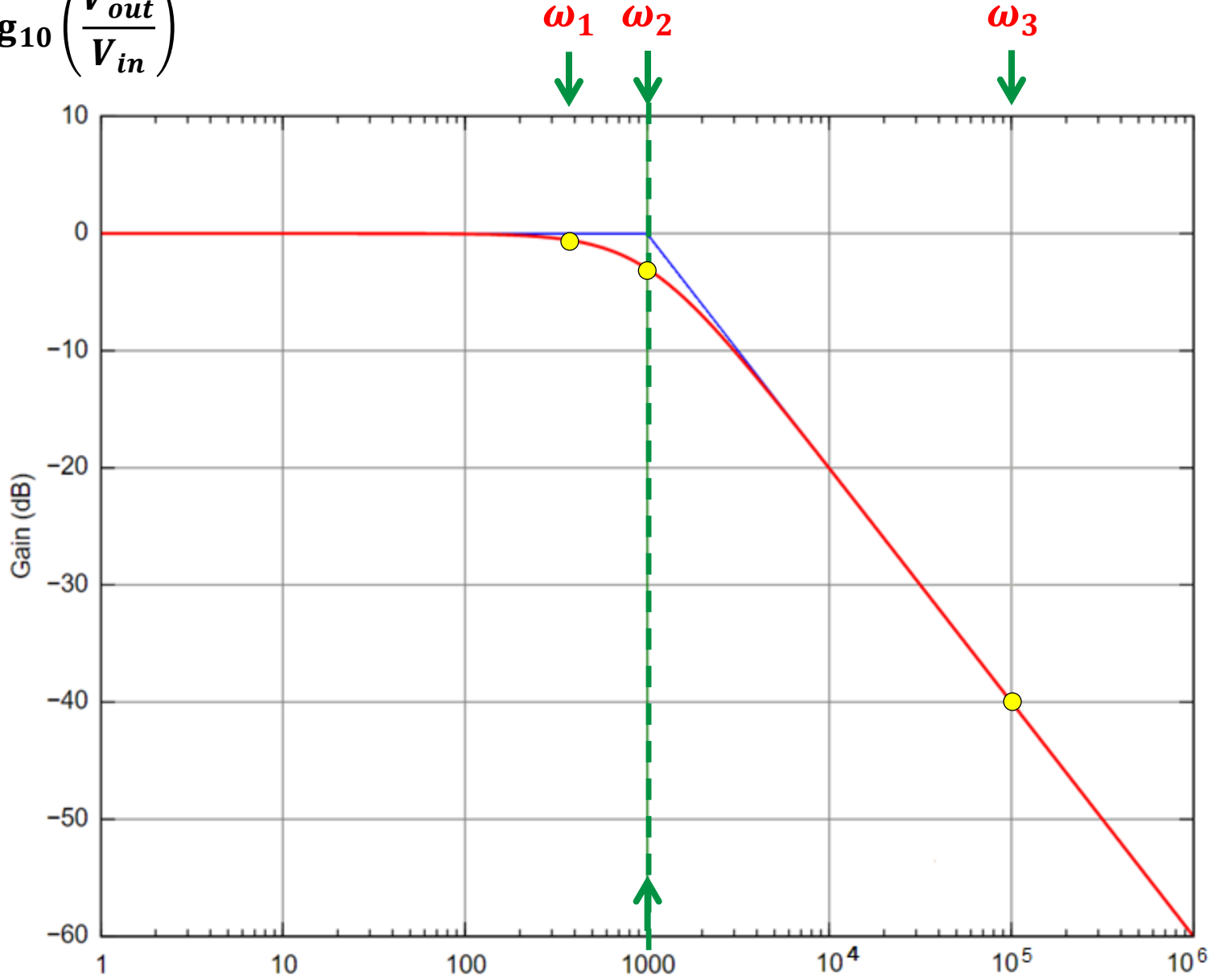
$$\omega_3 = 100,530 \text{ rad/s}$$

$$\omega_3 RC = 2\pi \times 16\text{k} \times 2.5\text{k} \times 400 \times 10^{-9} \approx 1.0$$

$$|H(\omega_3)| = \frac{1}{\sqrt{1 + (\omega_3 RC)^2}} = 0.7052$$

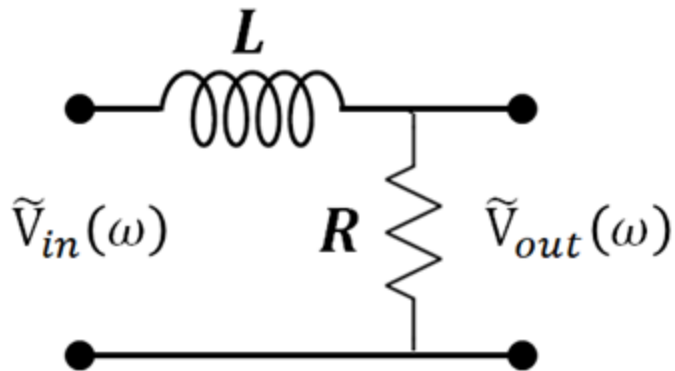
$$|H(\omega_3)|_{\text{dB}} = 20 \log_{10}(0.7052) = -40.046 \text{ dB}$$

$$20 \log_{10} \left(\frac{V_{out}}{V_{in}} \right)$$

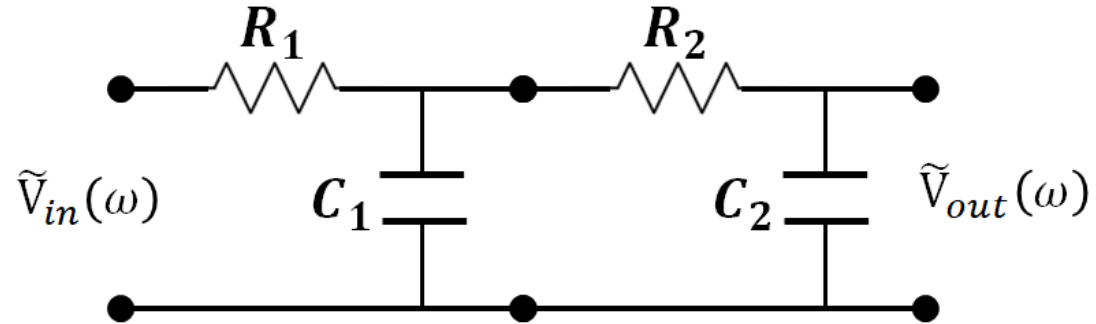


$$\omega_c = 2\pi f_c$$

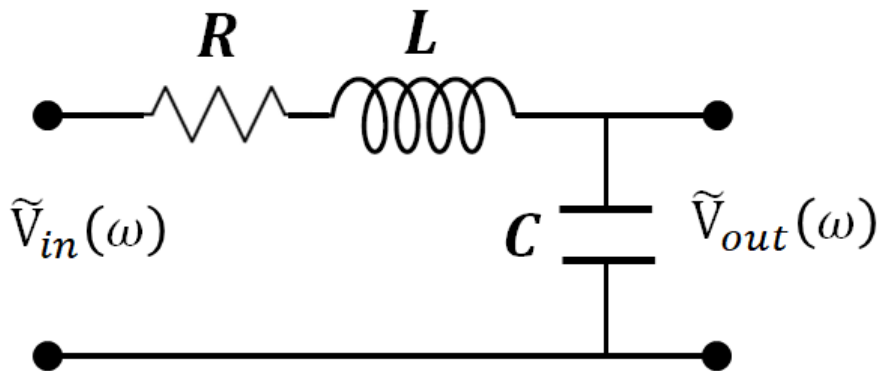
Other Low-Pass Passive filter configurations



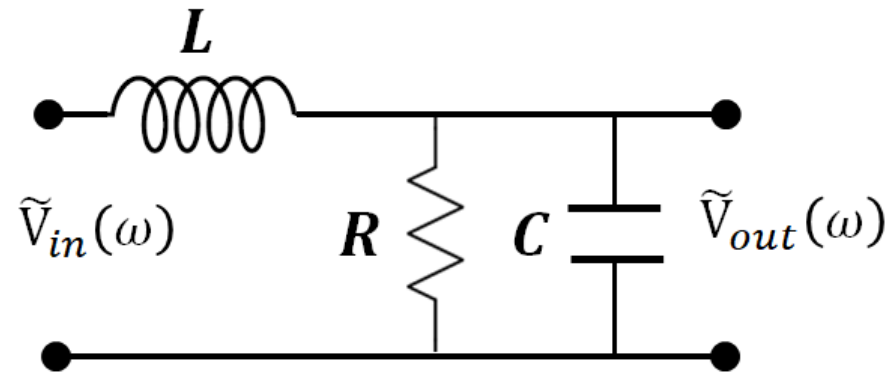
RL filter (1st order)



RC filter (2nd order)



RLC filter (2nd order)



RLC filter (2nd order)